



Stress Drop Variability

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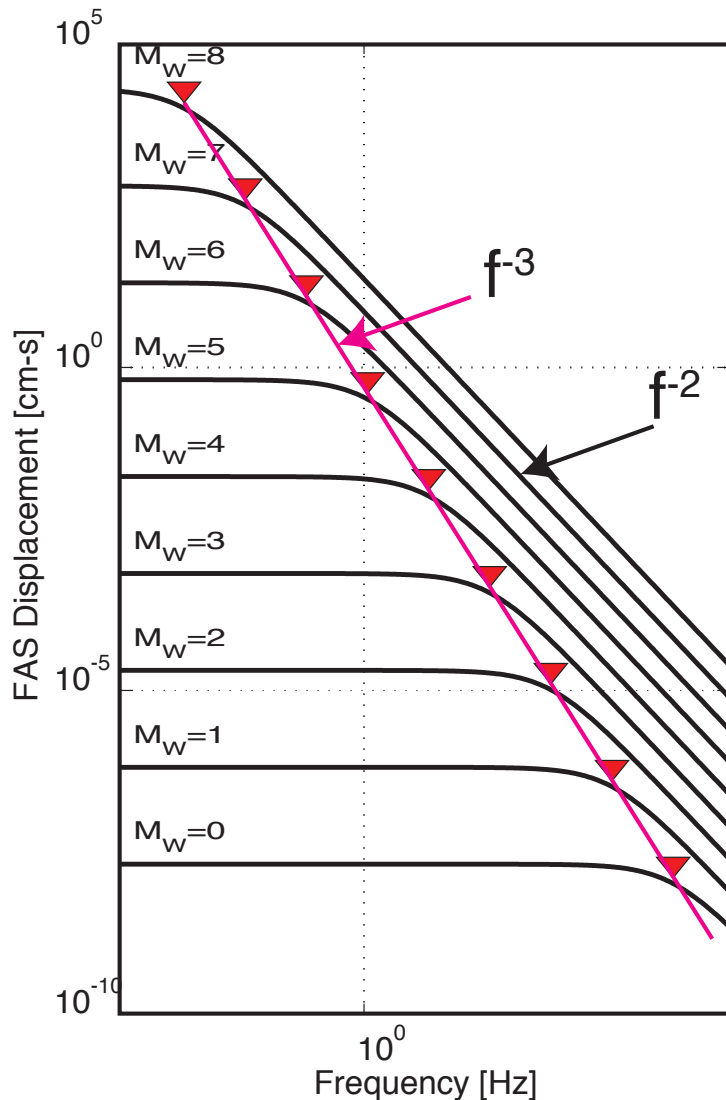
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Université Joseph Fourier, Grenoble**



Self-Similarity: Constant Stress Drop Aki (1967)

Aki's ω^{-2} Spectrum



$$|A(\omega)| = \frac{wD_0L}{\left\{1 + \left(\frac{\cos\theta}{C} - \frac{1}{V}\right)^2 \left(\frac{\omega}{k_L}\right)^2\right\}^{1/2} \left\{1 + \left(\frac{\omega}{k_L}\right)^2\right\}^{1/2}}$$

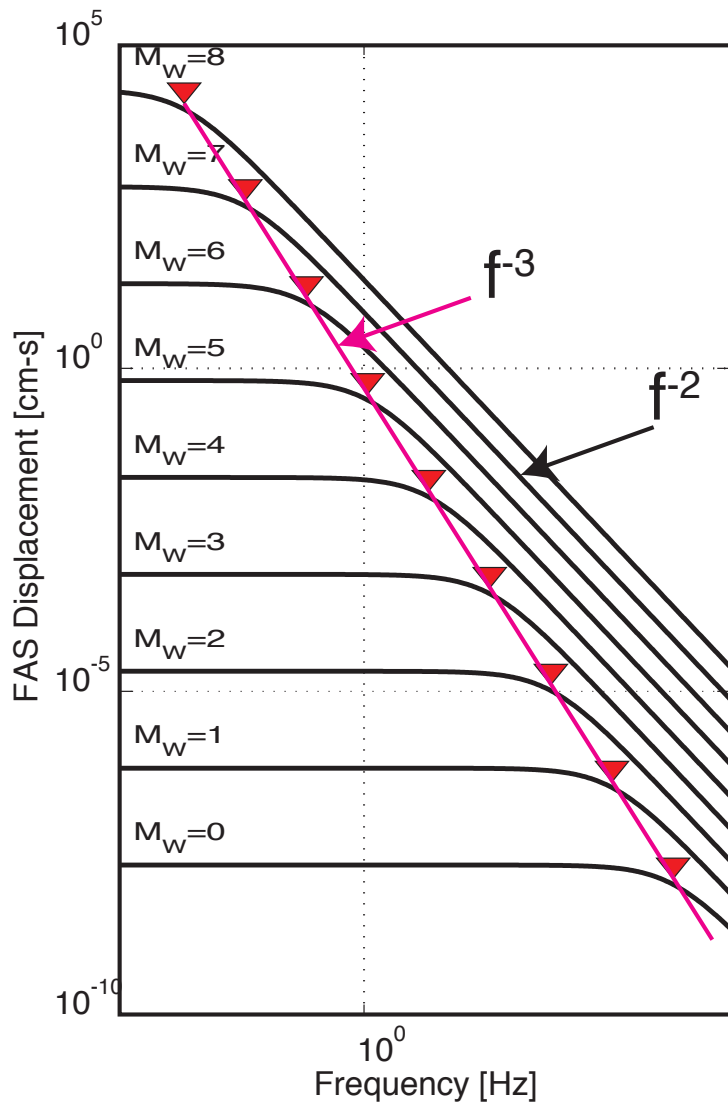
“Further, in order to specify an earthquake by a single source parameter, ‘magnitude,’ we must reduce to one the number of parameters appearing in (30) and (31) by assuming they are related to each other in some manner.

The simplest of such assumptions may be that large and small earthquakes are similar phenomena. If any two earthquakes are geometrically similar, the fault width w is proportional to the length L . If they are physically similar, all the nondimensional products formed by the source parameters will be the same. The average dislocation D_0 will be proportional to L and, consequently to w . This implies that if an earthquake is a Starr fracture, the pre-existing stress or strength is constant and independent of source size [Tsuboi, 1956].”



Self-Similarity: Constant Stress Drop Aki (1967)

Aki's ω^{-2} Spectrum



“Since the wave velocity is practically independent of source and may be considered constant for our present purpose, all the quantities having the dimension of velocity must also be constant and independent of source size. Thus, the similarity assumptions imply that the rupture velocity v is a constant and that all the quantities having the dimension of time, such as, k_T^{-1} and $(vk_L)^{-1}$ are proportional to L .”

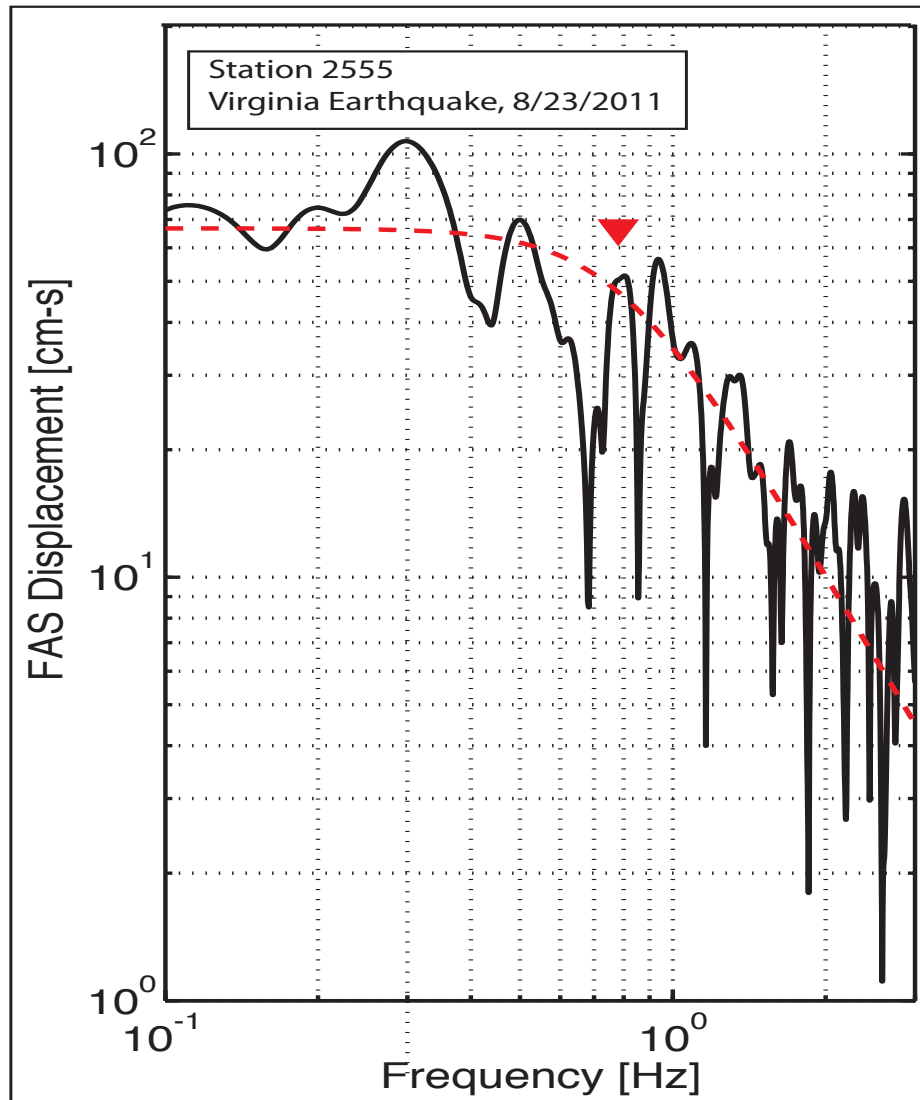
From dimensional analysis

$$\frac{D}{L} = \gamma \frac{\Delta\tau}{\mu}$$

$$\frac{\dot{D}}{L} = \zeta \frac{\Delta\tau}{\mu} V_s$$



Spectra and Corner Frequency: Brune (1970)



The average spectrum is given by:

$$\langle \Omega_s(\omega) \rangle = \langle R_{\theta\theta} \rangle (\sigma\beta / \mu) (r/R) (\omega^2 + (2.36\beta/r)^2)^{-1}$$

The corner frequency $f_c = (1/2\pi)(2.36\beta/r) = 0.37\beta/r$

At zero frequency, the spectrum must be the same as that from the double-couple dislocation.

$$\langle \Omega_s(0) \rangle = \langle R_{\theta\theta} \rangle M_0 / (4\pi\rho\beta^3 R)$$

or

$$M_0 = (4\pi\rho\beta^3 R) \langle \Omega_s(0) \rangle / \langle R_{\theta\theta} \rangle$$

Brune (1970, 1971): $f_c = 0.37\beta/r$

Madariaga(1976) $f_c = 0.21\beta/r$

Madariaga(1979) $f_c = 0.28\beta/r$



Stress Drop and Moment

Static Stress Drop and Seismic Moment for Three Fault Geometries

	Circular (Radius, r)	Strike-Slip (Width, W)	Dip-Slip (Width, W)
$\Delta\tau$	$\left(\frac{7\pi}{16}\right)\mu\left(\frac{\bar{D}}{r}\right)$	$\left(\frac{2}{\pi}\right)\mu\left(\frac{\bar{D}}{W}\right)$	$\left(\frac{4}{\pi}\right)\left(\frac{\lambda+\mu}{\lambda+2\mu}\right)\mu\left(\frac{\bar{D}}{W}\right)$
M_0	$\left(\frac{16}{7}\right)\Delta\tau r^3$	$\left(\frac{\pi}{2}\right)\Delta\tau W^2 L$	$\left(\frac{\pi}{4}\right)\left(\frac{\lambda+2\mu}{\lambda+\mu}\right)\Delta\tau W^2 L$

Moment: Aki (1966)

Slip related to a source dimension:

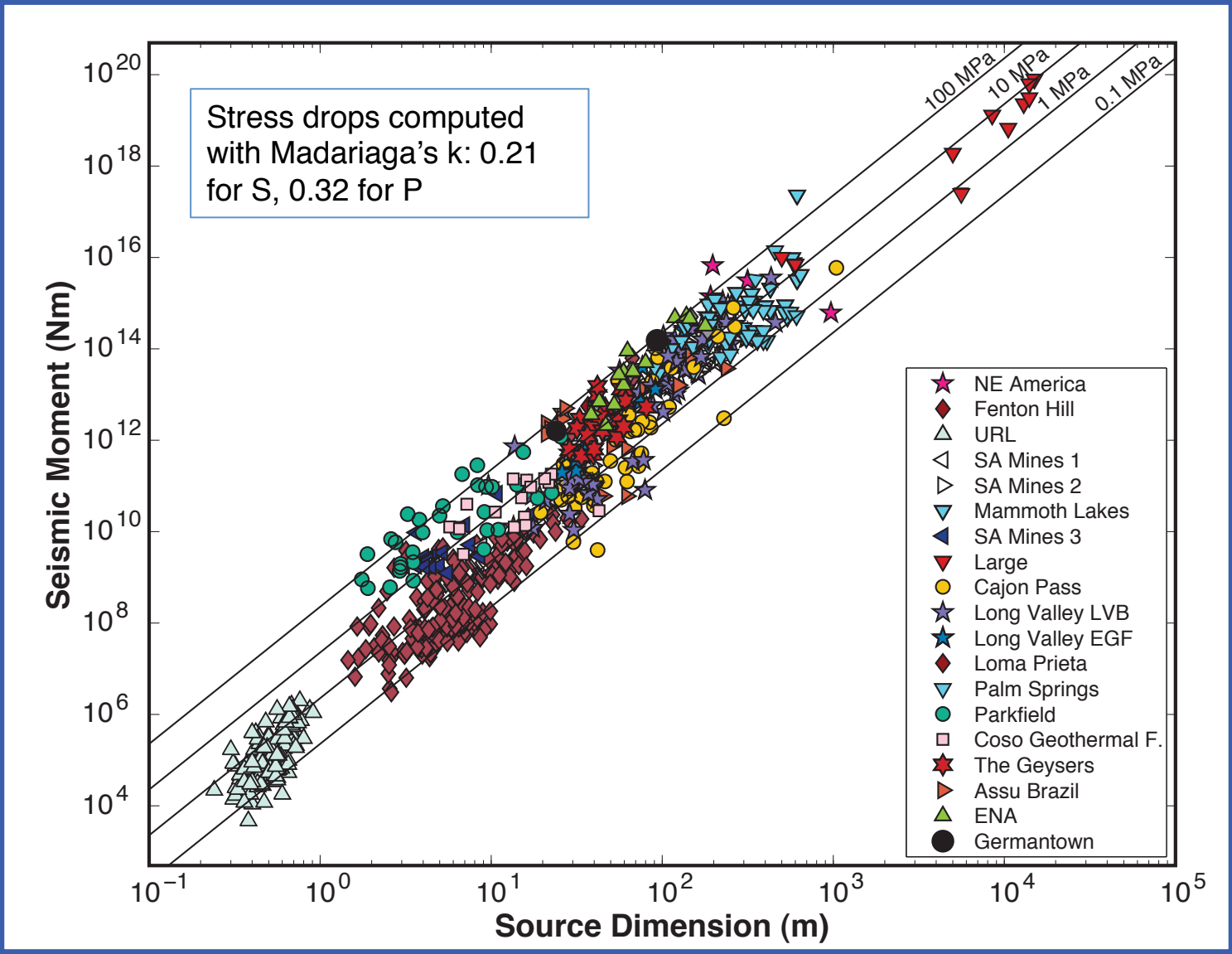
Eshelby (1957)

Knopoff (1958)

Starr (1928)

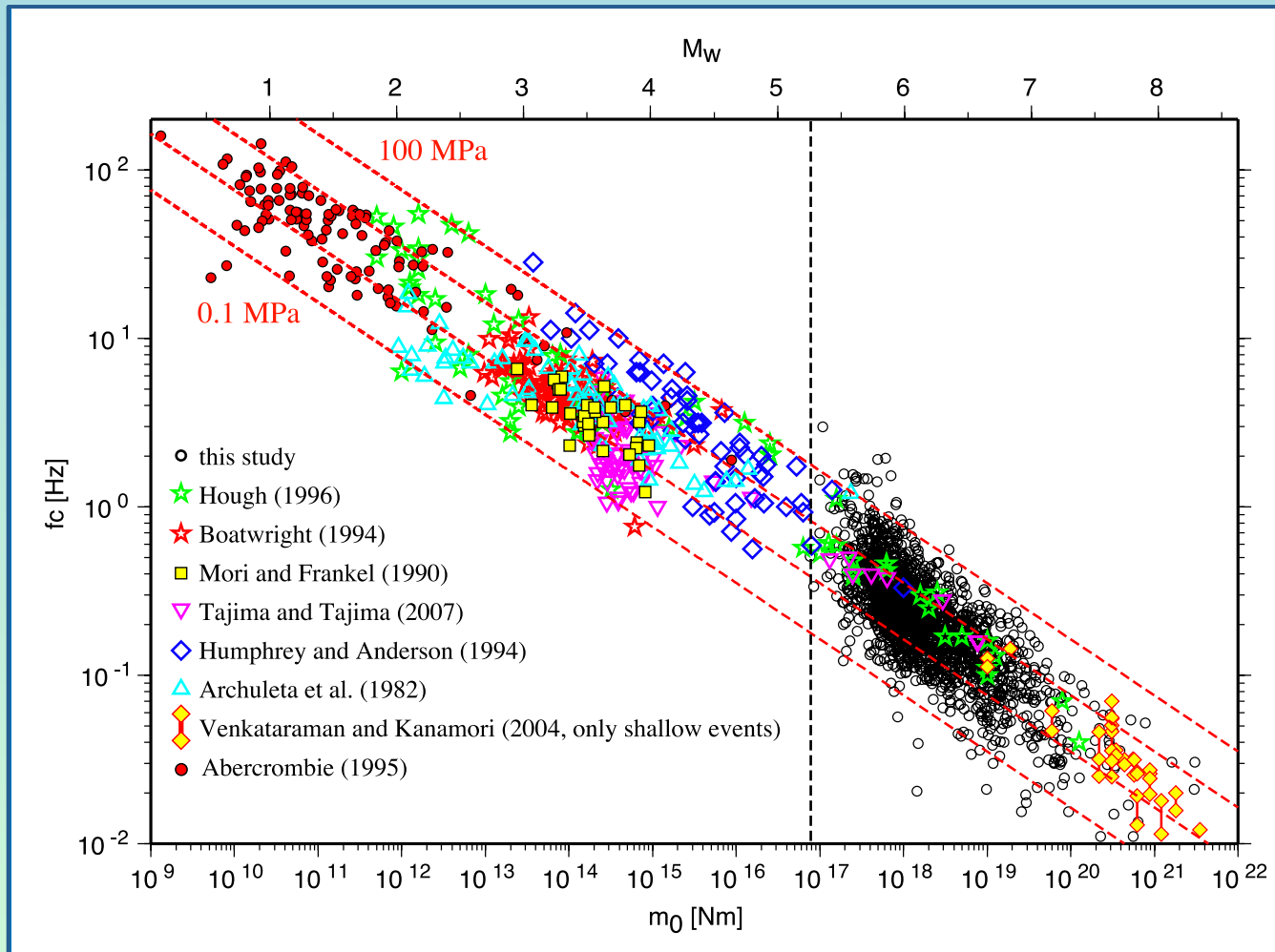


Stress Drops



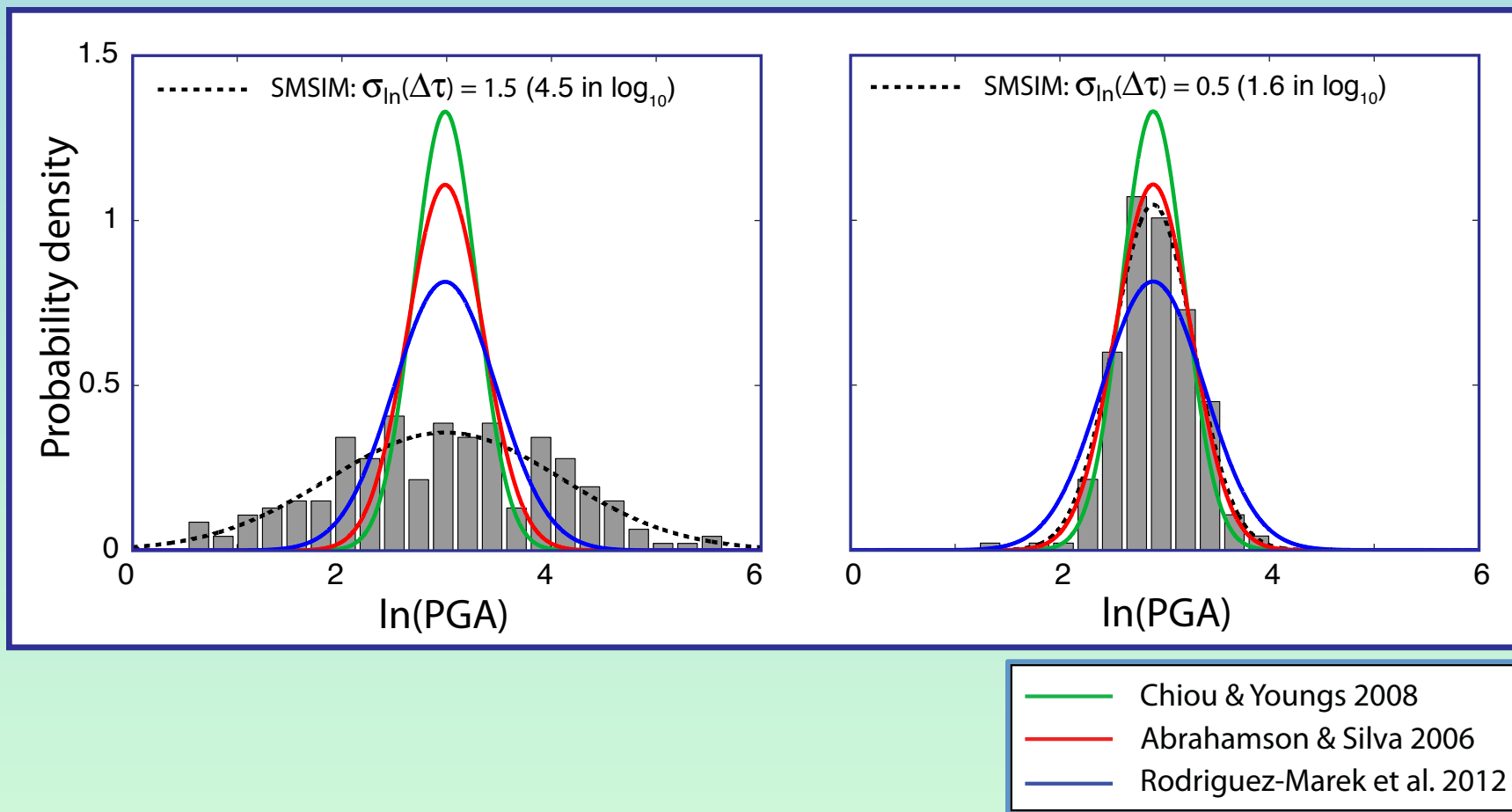


Stress Drop: $10^9 \leq M_0 \leq 10^{22}$ Nm





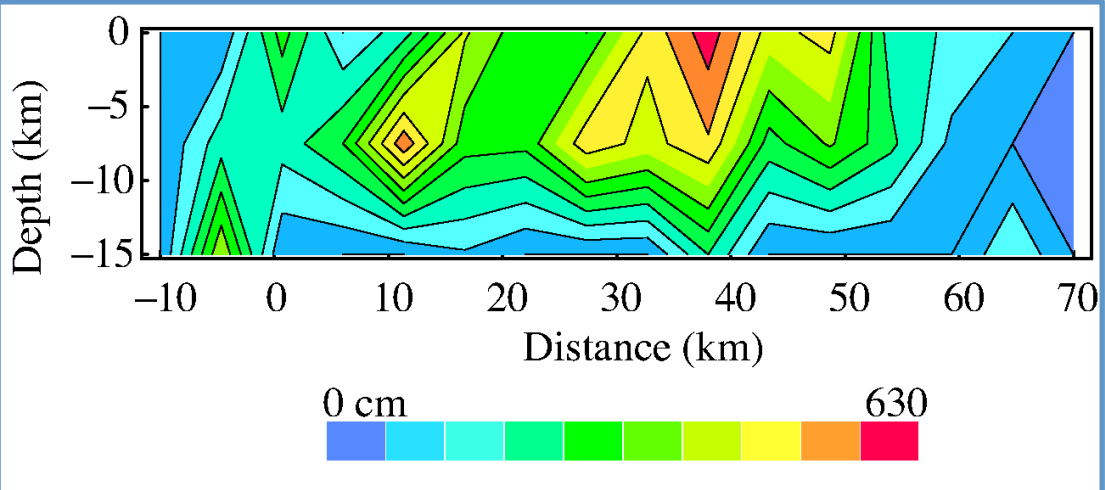
Sigma: Its Effect on Ground Motion



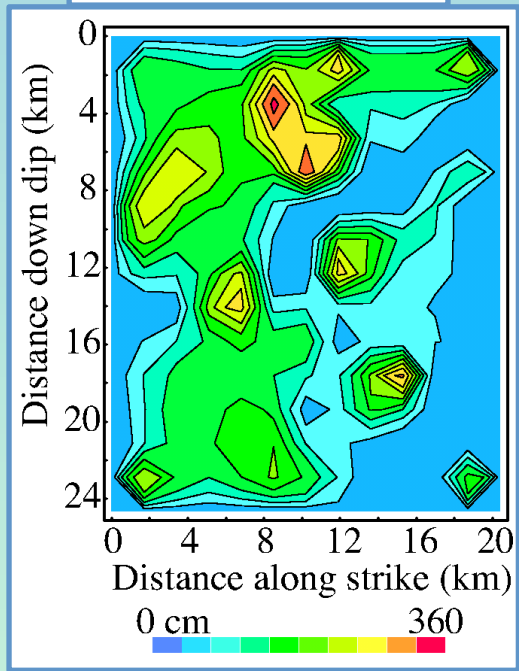


Heterogeneous Slip (Stress)

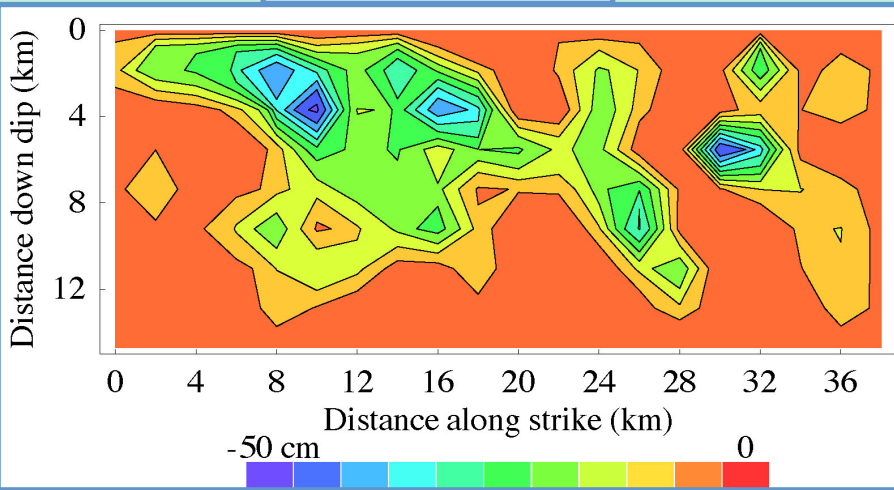
Landers 1992



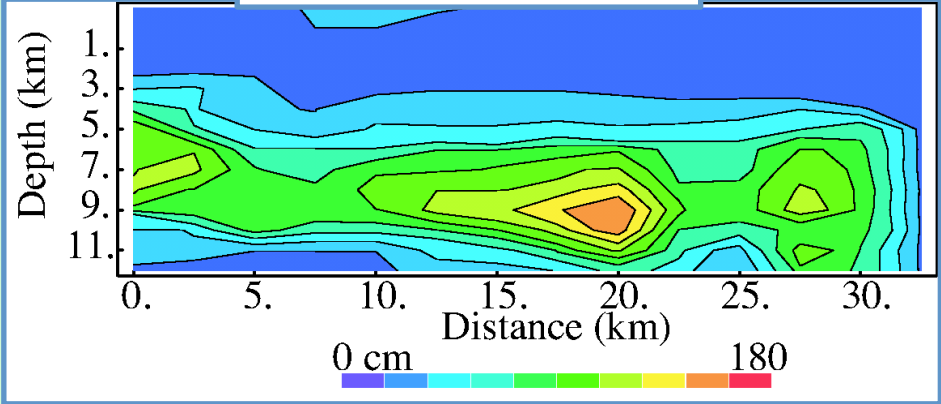
Northridge 1994



Parkfield 2004

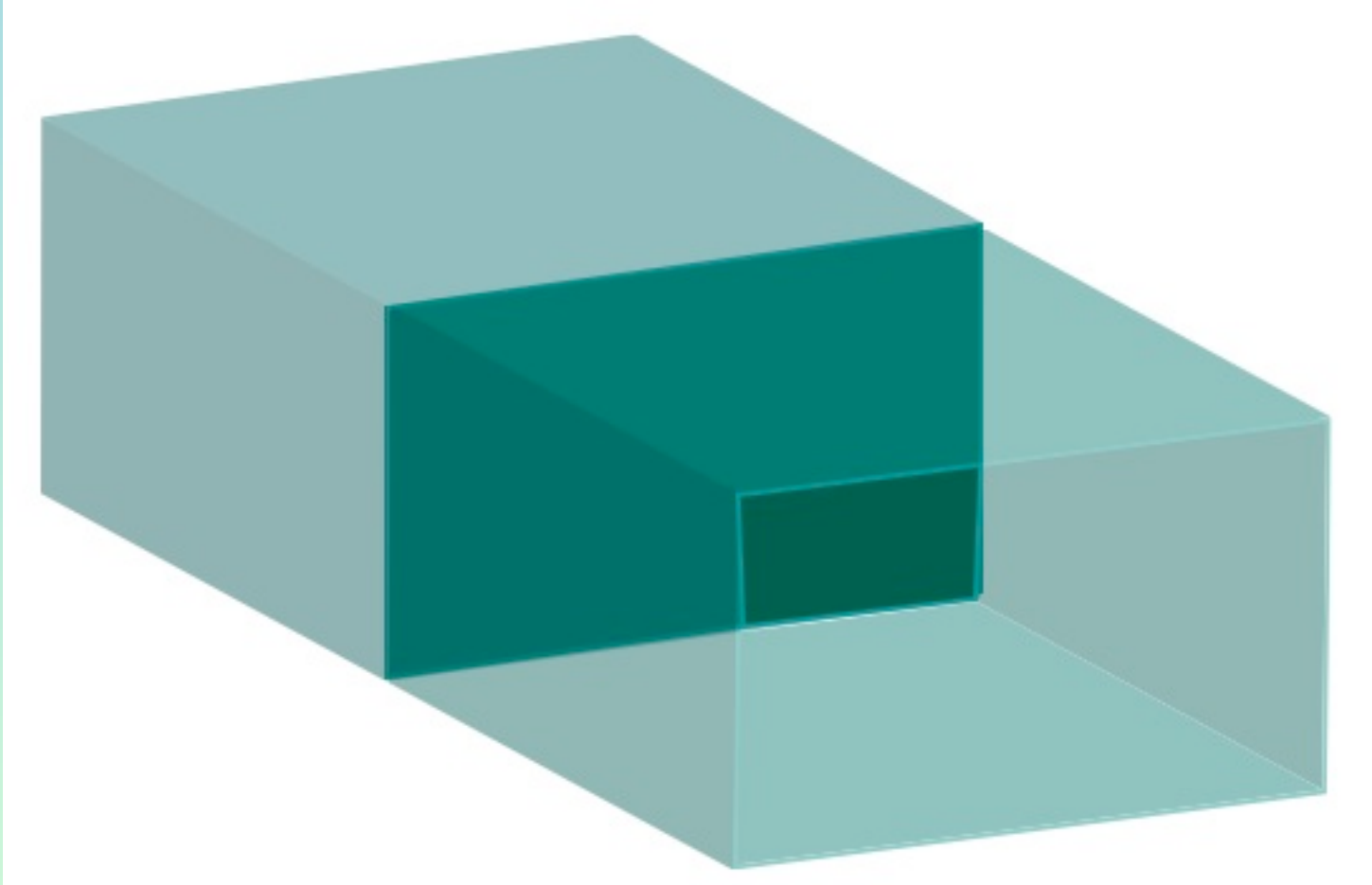


Imperial Valley 1979



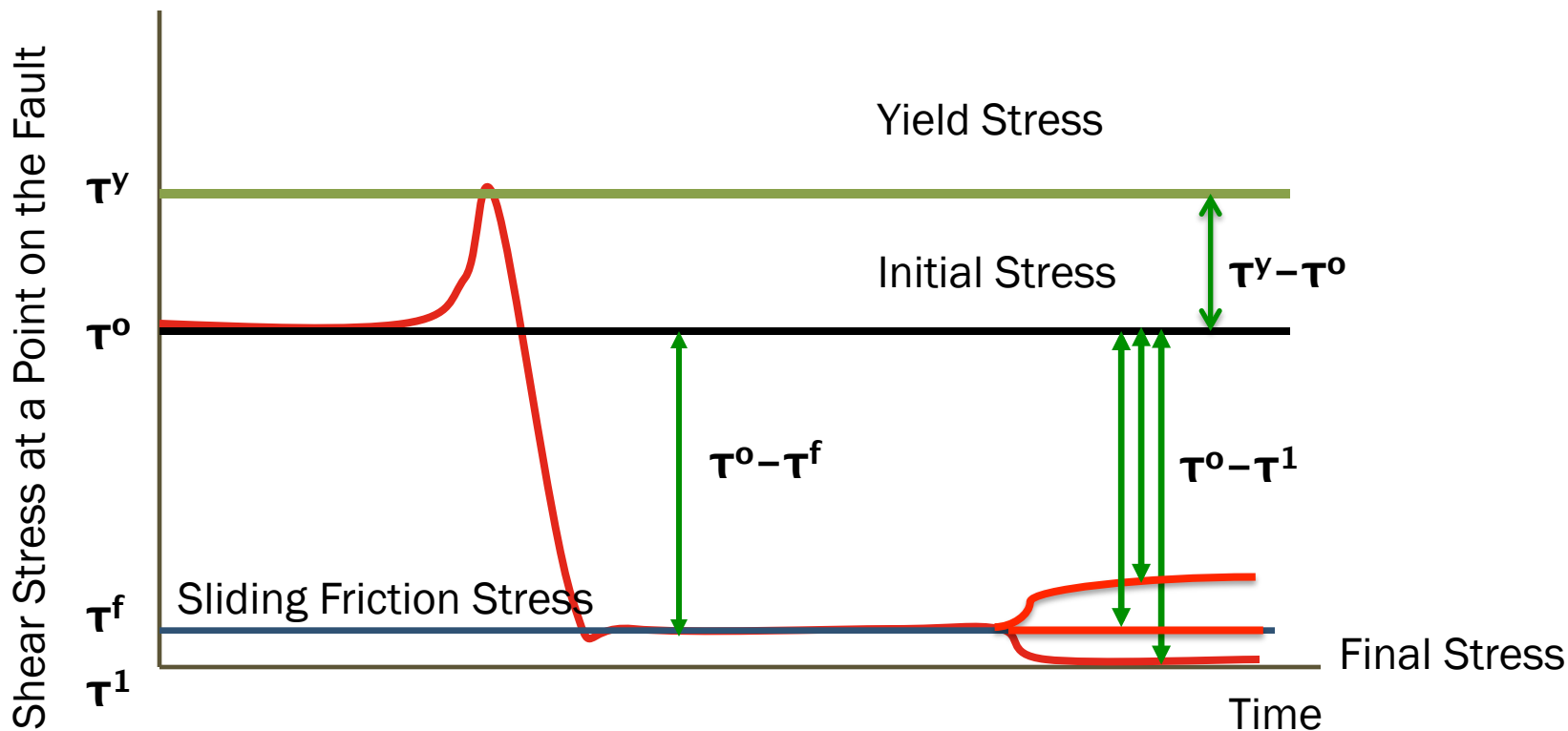


Fault in Homogeneous Medium





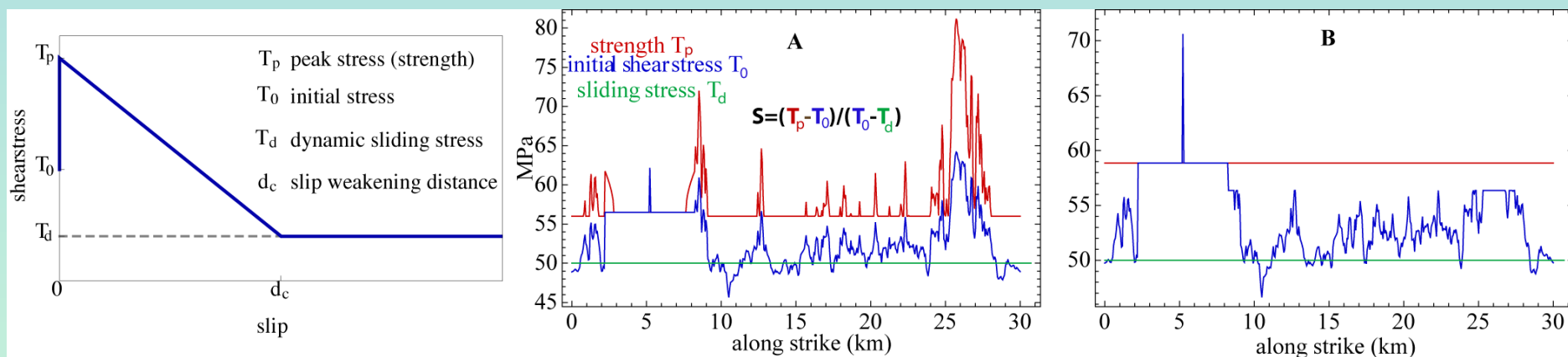
Stress at a Point on the Fault



$$S = \tau^y - \tau^0 / \tau^0 - \tau^f = \text{Strength Excess/Stress Drop}$$



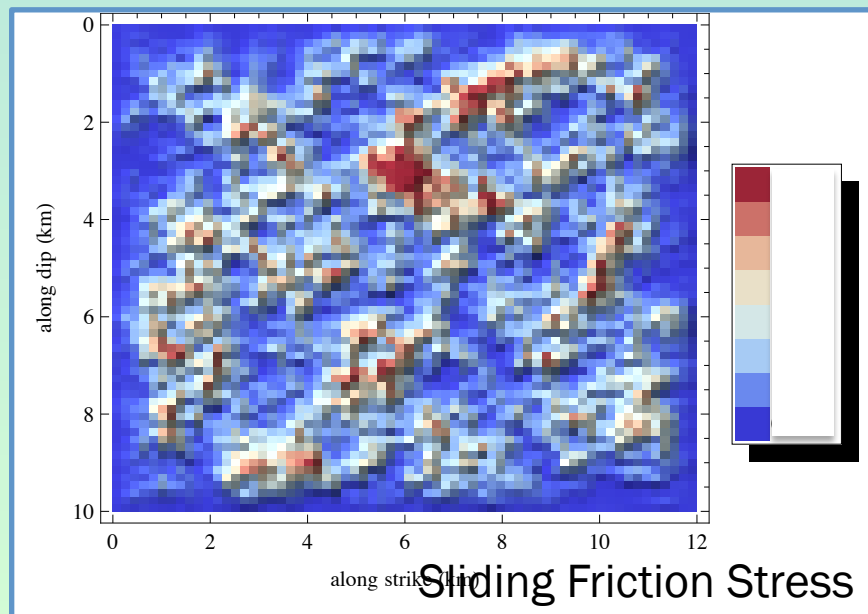
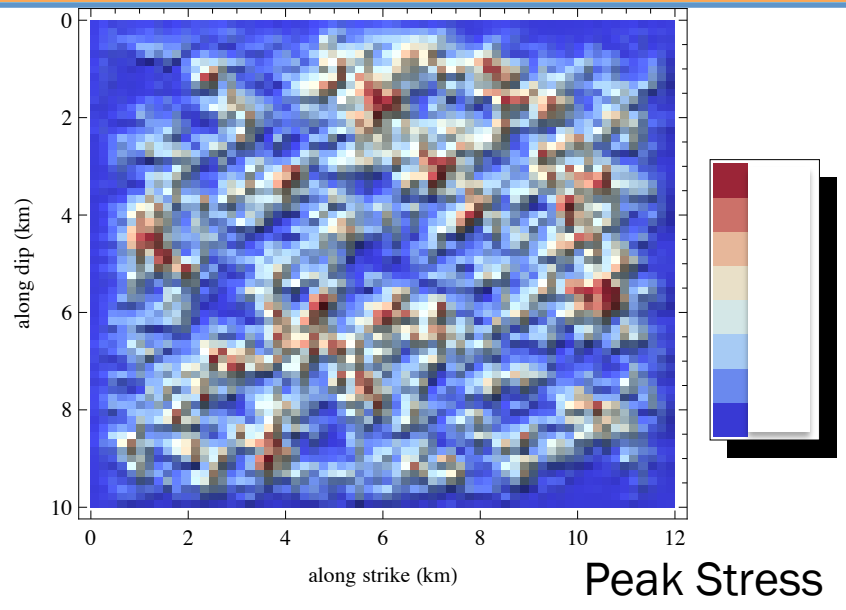
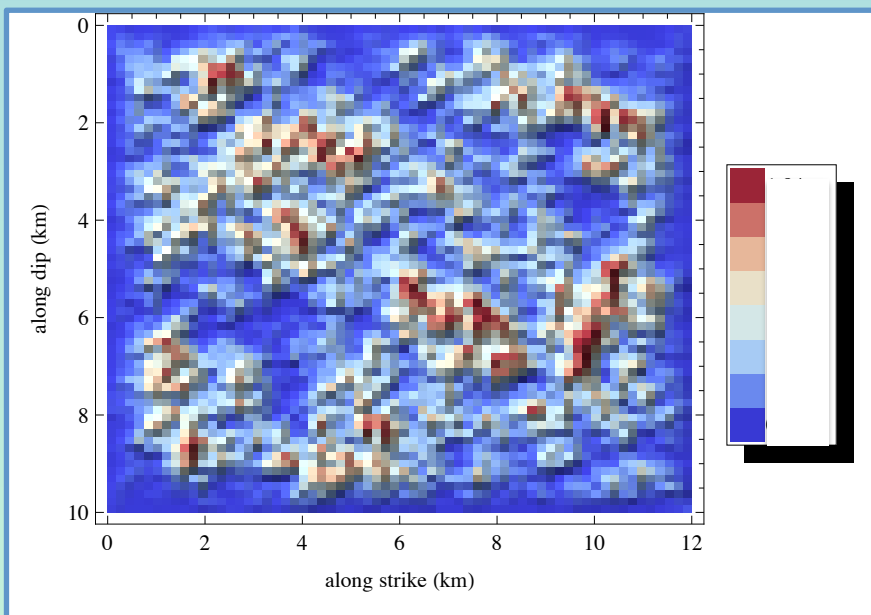
Stress and Dynamics





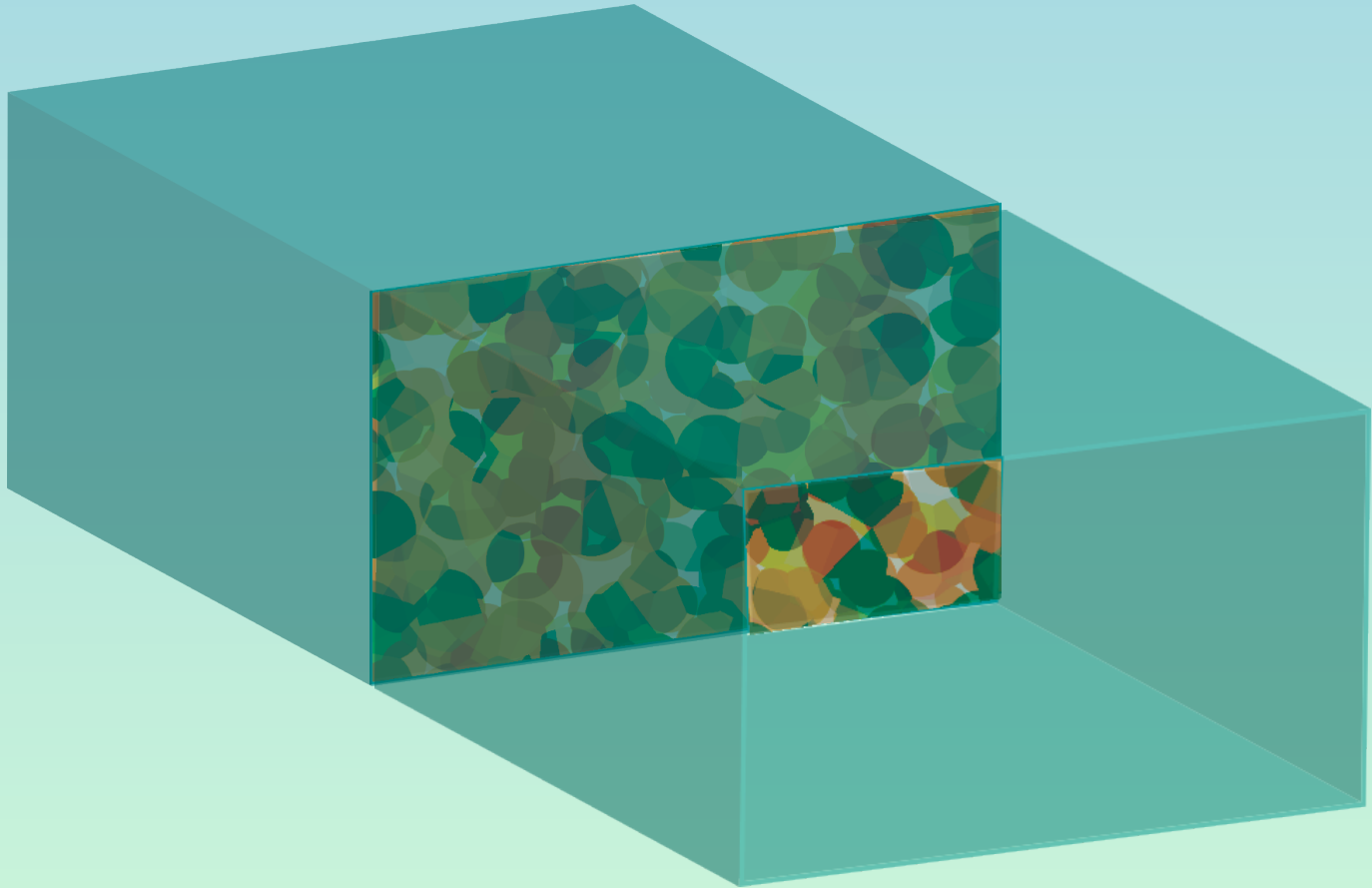
Stress and Dynamics

Initial Stress



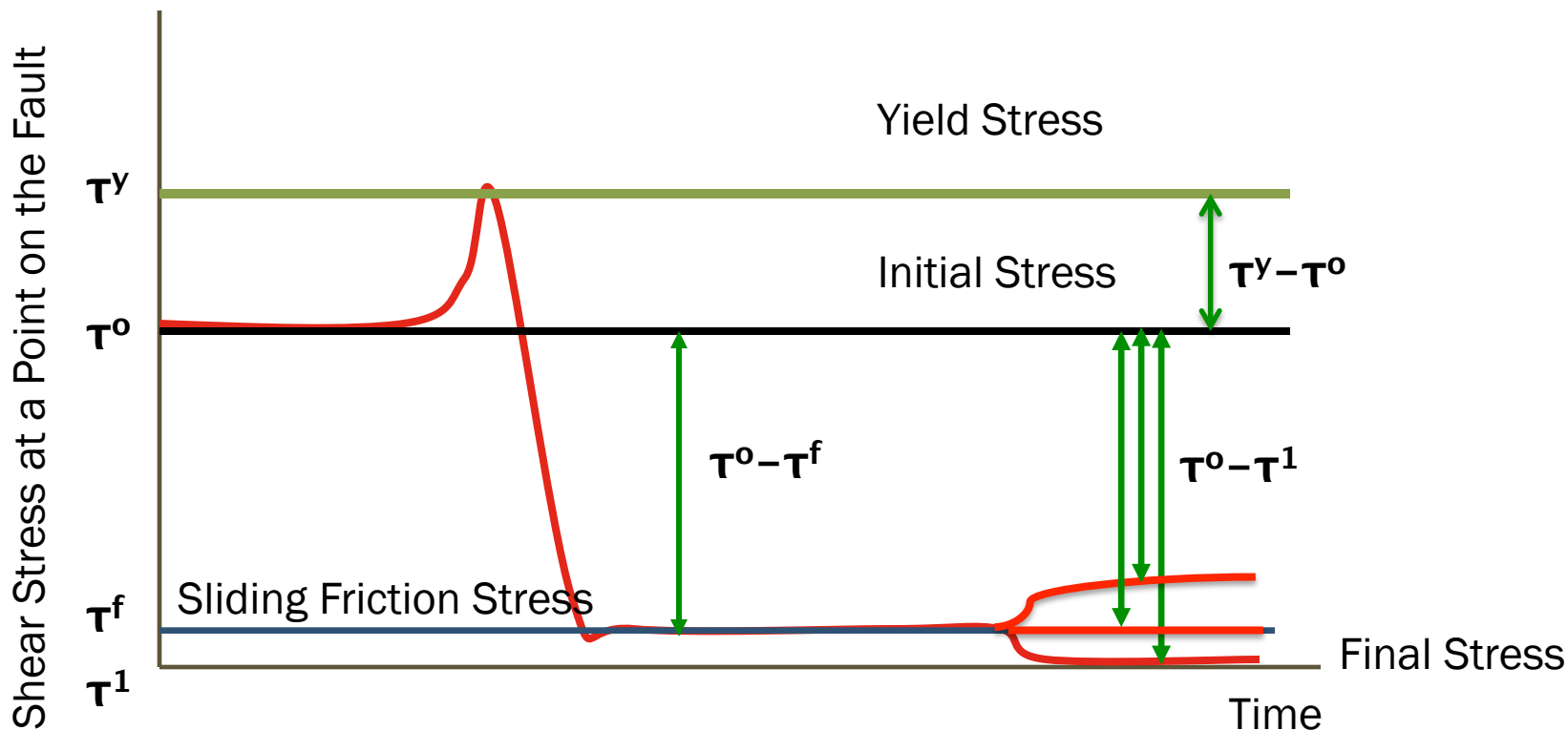


Fault in Heterogeneous Medium





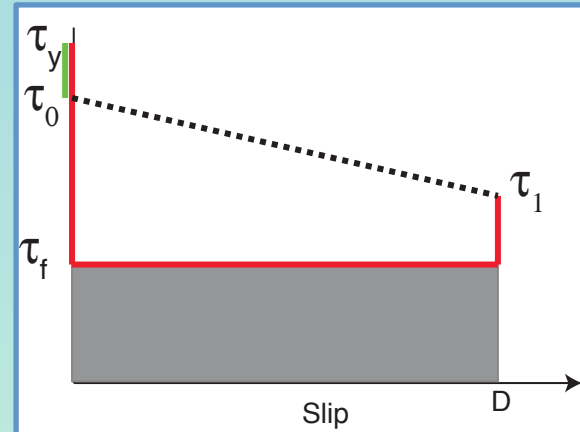
Stress at a Point on the Fault



$$S = \tau^y - \tau^0 / \tau^0 - \tau^f = \text{Strength Excess/Stress Drop}$$



Static Stress Drop, Stress Drop, Apparent Stress



$$\Delta W = \frac{\tau_0 + \tau_1}{2} DA = \frac{1}{\mu} \frac{\tau_0 + \tau_1}{2} \mu DA = \frac{1}{\mu} \frac{\tau_0 + \tau_1}{2} M_0 = \frac{1}{\mu} \bar{\tau} M_0$$

$$\bar{\tau} = \frac{\mu \Delta W}{M_0}$$

If frictional work is zero, the change in potential energy ΔW goes entirely into radiated energy E_R . When the radiation efficiency is not equal to 1, then

$$\bar{\tau} = \frac{\mu \Delta W}{\eta M_0} = \frac{\tau_a}{\eta} \quad \text{where } \eta \text{ is the radiation efficiency: } E_R = \eta \Delta W.$$

We could also write

$\Delta W = E_R + E_f$ where $E_f = \tau_f DA$ the energy lost to friction with τ_f the stress at sliding friction.

$$\bar{\tau} = \frac{\mu}{M_0} (E_R + \tau_f DA) = \tau_a + \tau_f$$

$$\text{Since } \bar{\tau} = \frac{1}{2}(\tau_0 + \tau_1) = \frac{1}{2}(\tau_0 + \tau_0 - \Delta\tau_S) = \tau_0 - \frac{\Delta\tau_S}{2} \quad \text{where } \Delta\tau_S = \tau_0 - \tau_1$$

$$\tau_a = \bar{\tau} - \tau_f = \tau_0 - \tau_f - \frac{\Delta\tau_S}{2}$$

$$\tau_a = \Delta\tau_d - \frac{\Delta\tau_S}{2}$$

where $\Delta\tau_d$ is the dynamic stress drop $\Delta\tau_d = \tau_0 - \tau_f$ and τ_a is the apparent stress.



Scaling Between f_c and r

$$f_c = k V_s / r$$

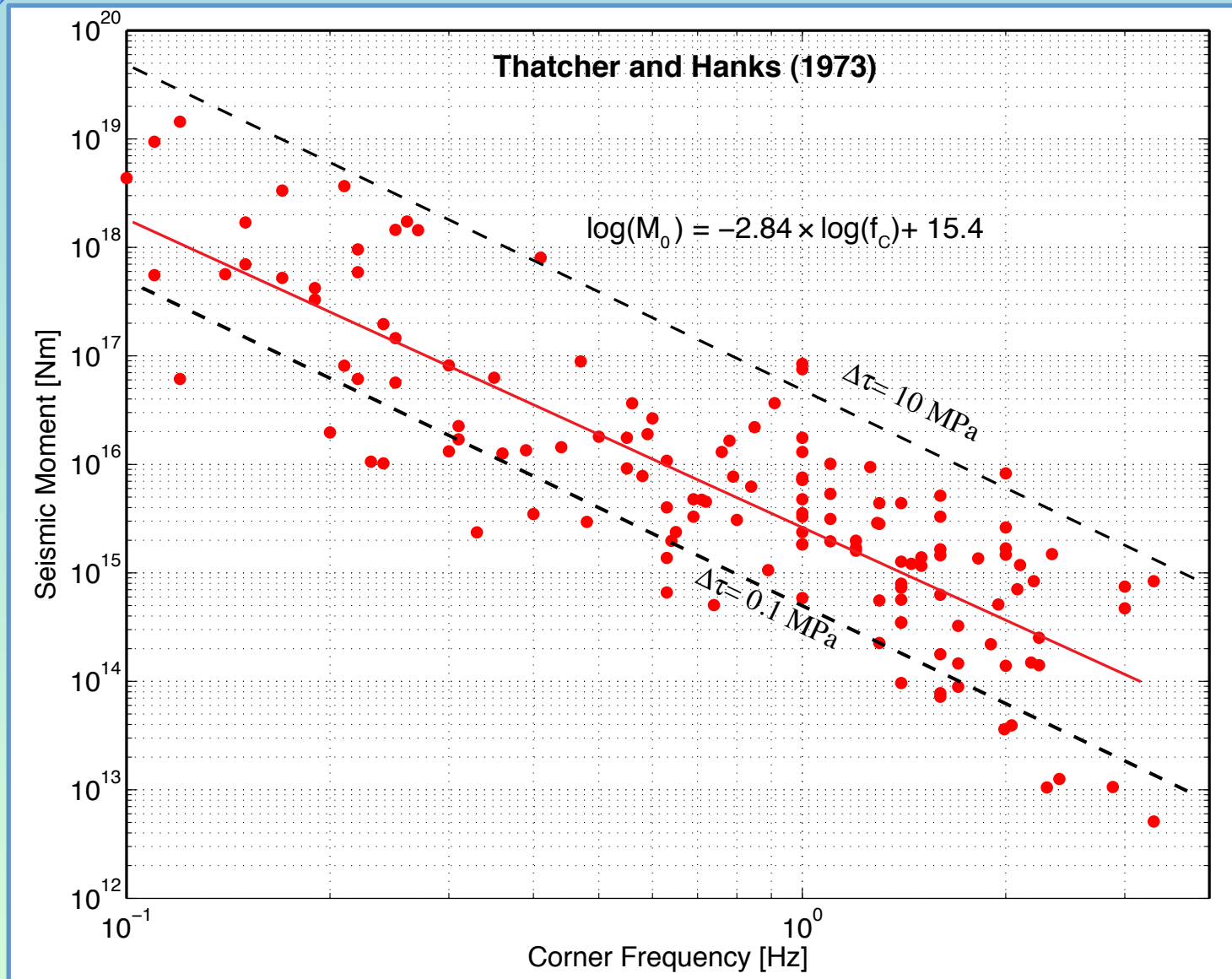
$$\Delta\tau = 7 M_0 / 16 r^3 = 7 M_0 f_c^3 / 16 (k V_s)^3$$

	V/V _s	C _p	C _s	k=(C _s /2π)	Multiplier on stress drop
Andrews*	0.90	1.55	2.86	0.46	0.52
Snoke*	0.90	1.73	2.83	0.45	0.56
Silver*	0.90	2.79	3.65	0.58	0.26
Sato & Hirasawa (1973)	0.90	1.6	1.99	0.32	1.55
Madariaga (1976)	0.90	(3/2)C _s —Use V _s	1.32	0.21	5.47
Kaneko & Shearer (2012)	0.90	0.38—Use V _s	1.63	0.26	2.88
Brune (1970, 1971)			2.32	0.37	1.0

* Dong and Papageorgiou, BSSA 2002

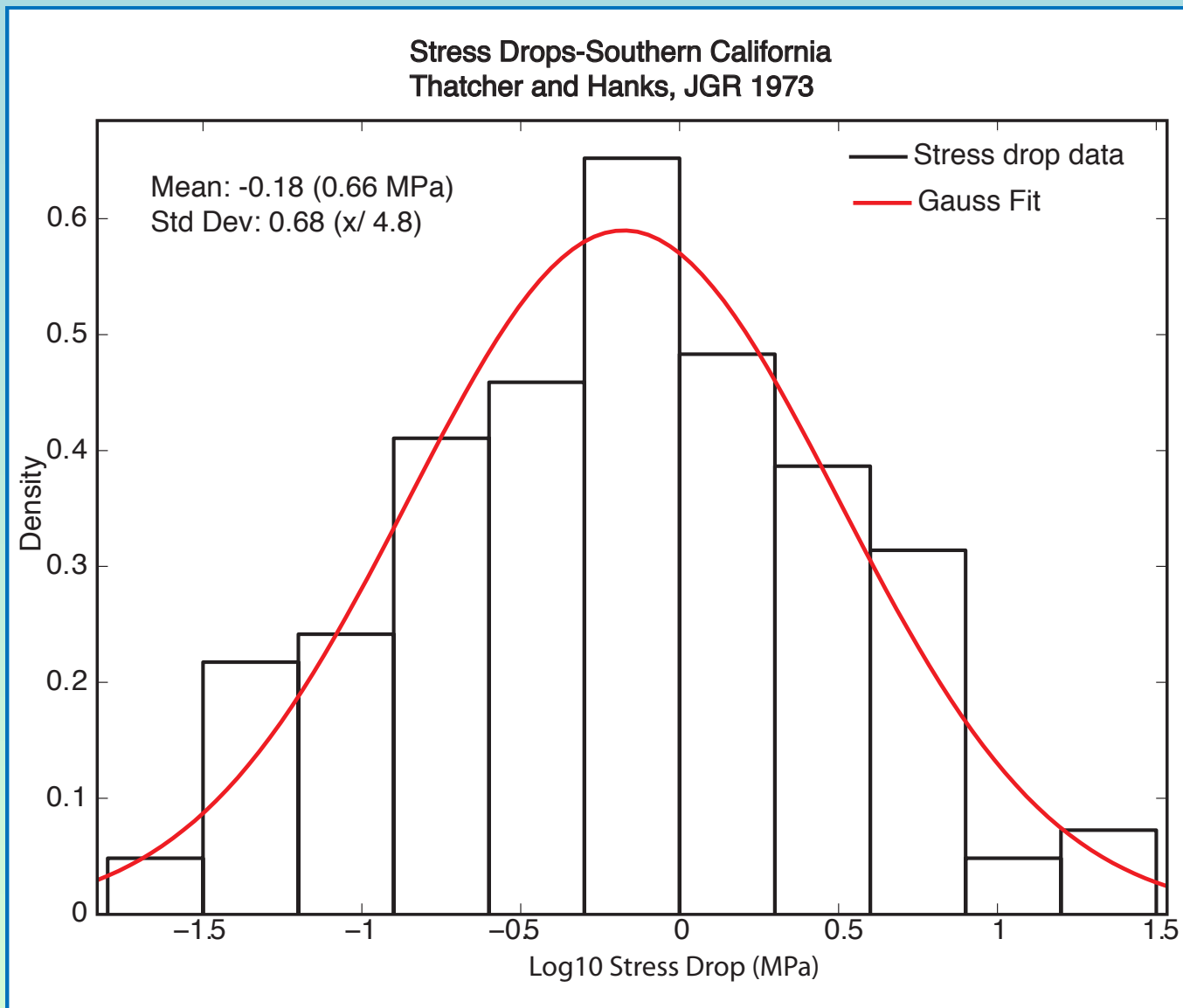


Southern California: M_0 vs f_c



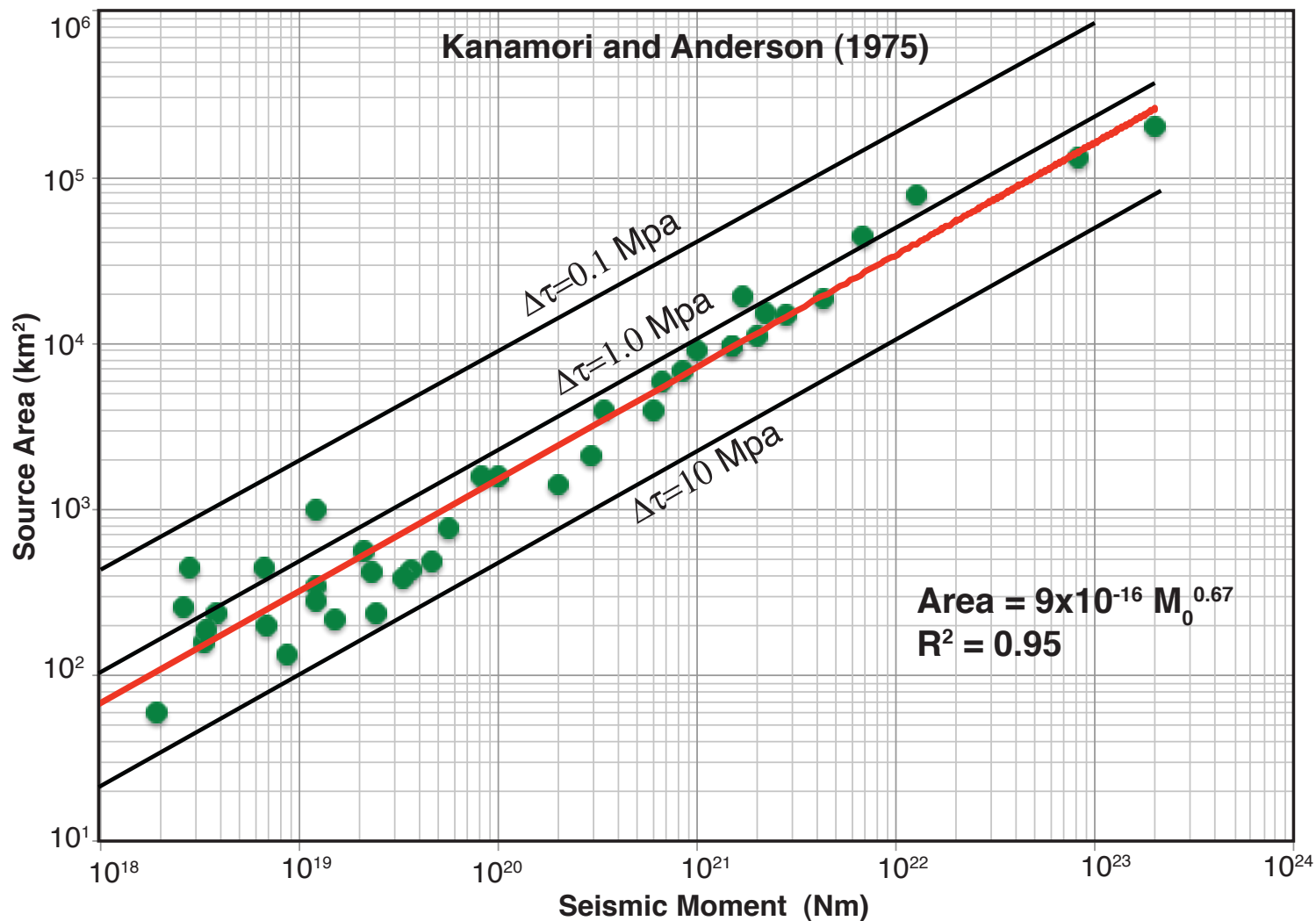


Brune Stress Drops: Southern California



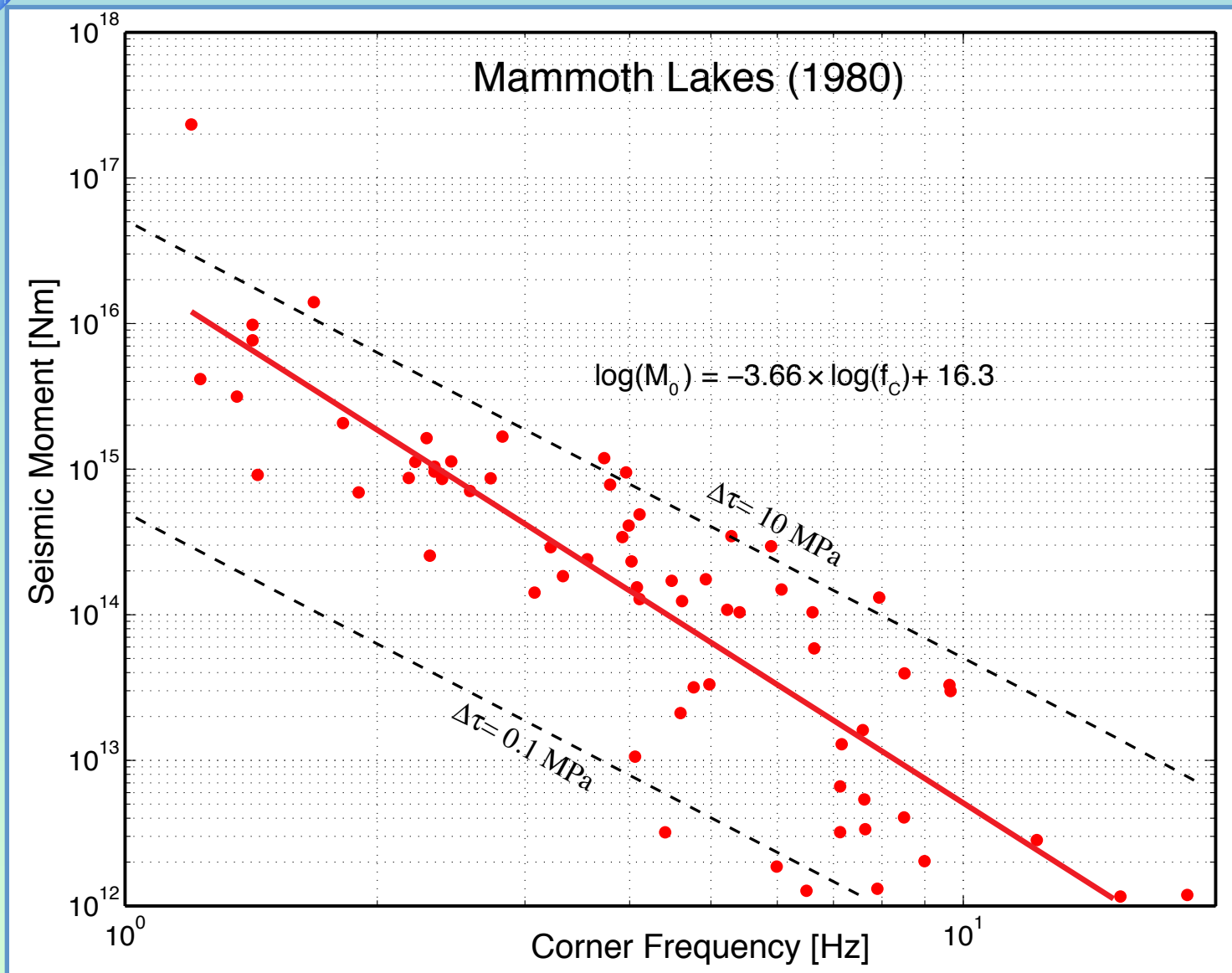


Stress Drop Based on Area-Moment



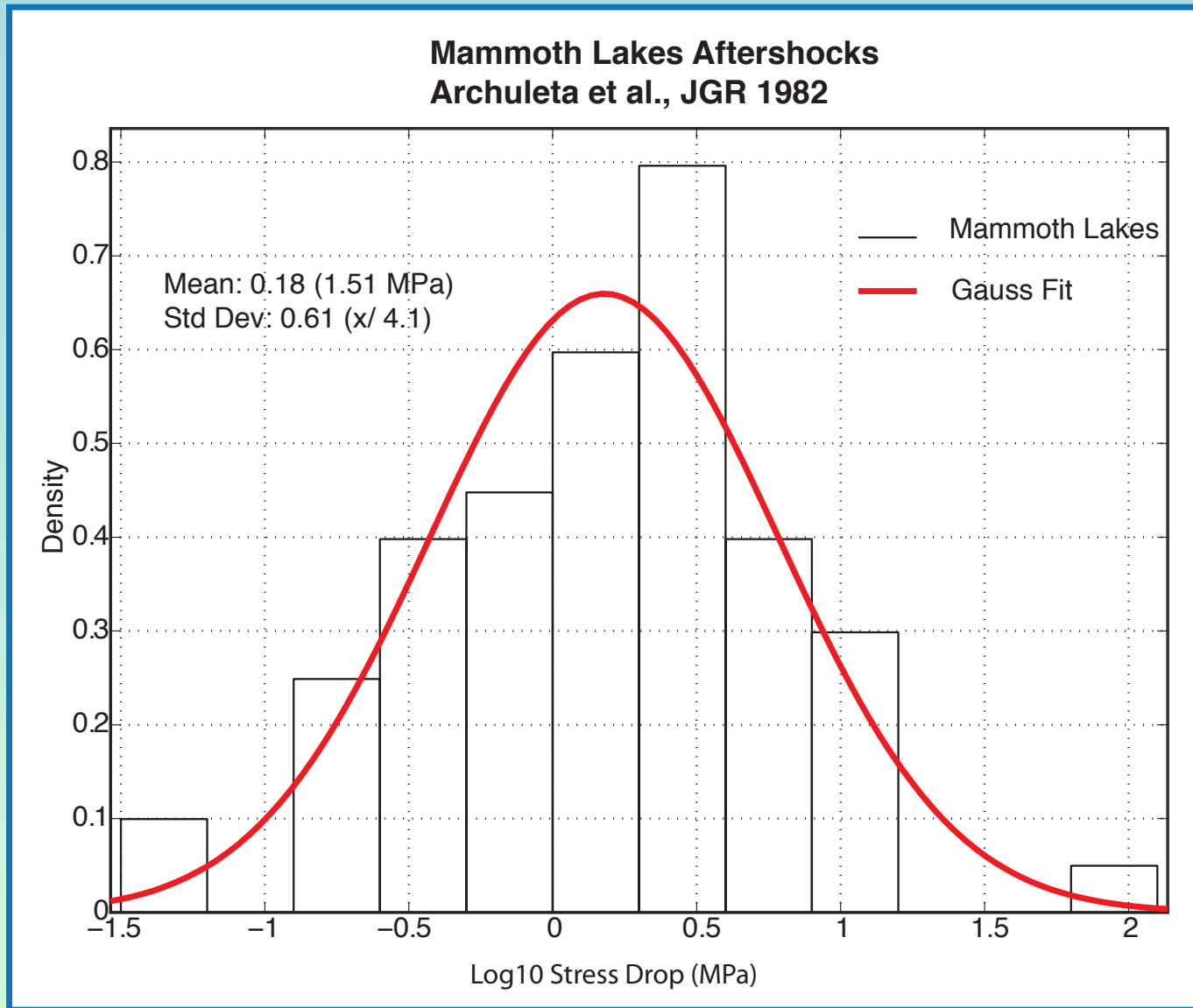


Mammoth Lakes: M_0 vs f_c



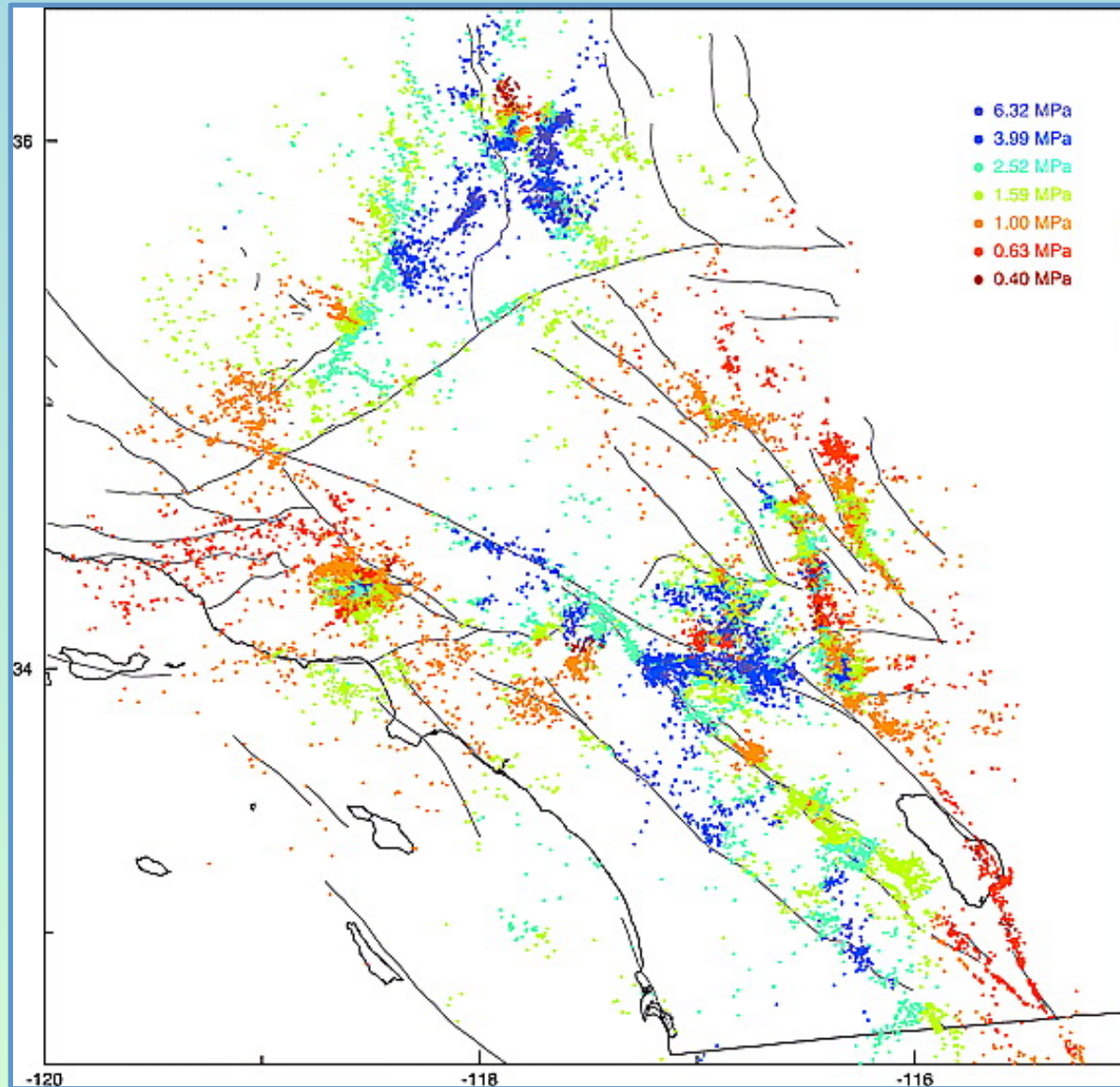


Brune Stress Drops: Mammoth Lakes



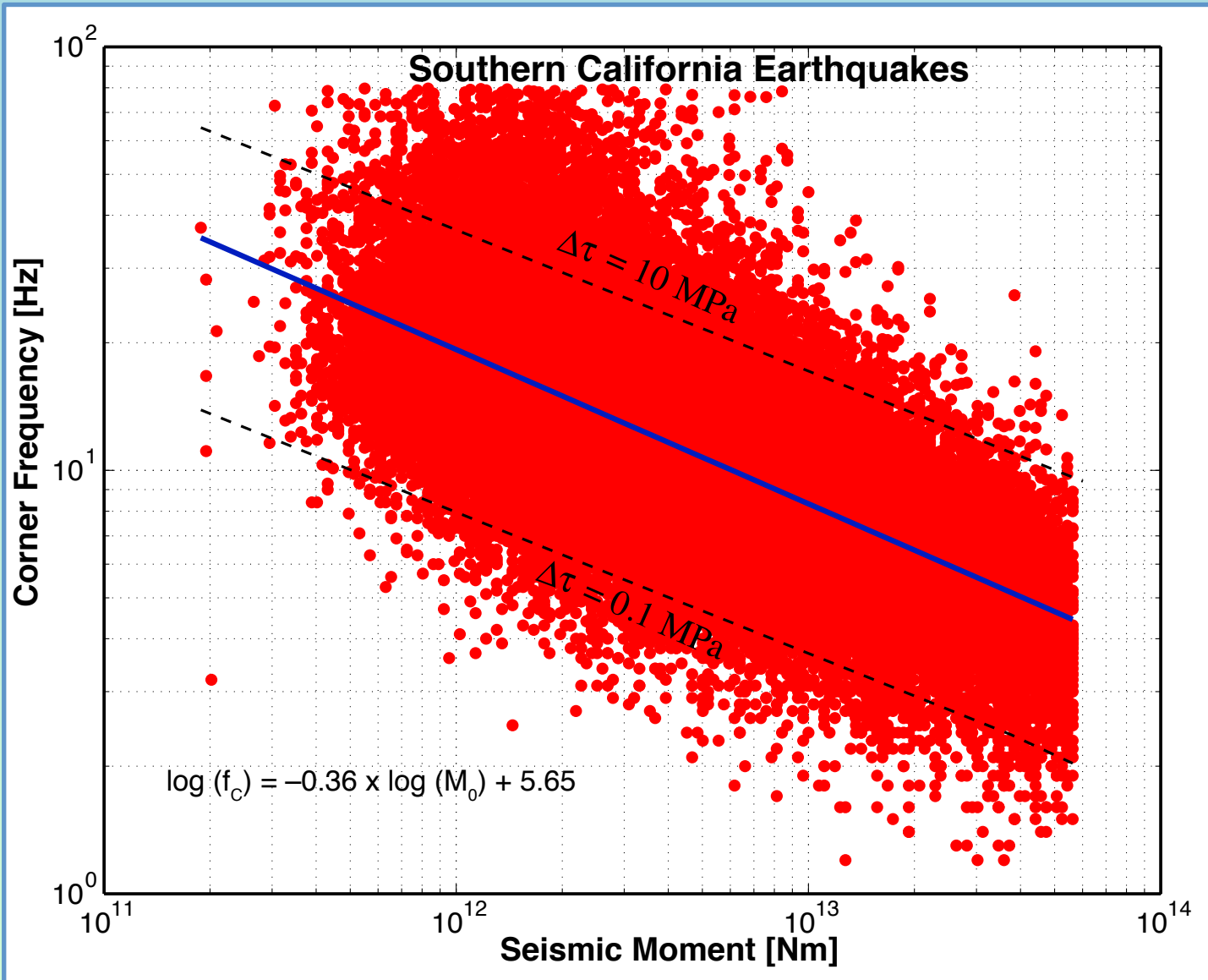


Southern California Stress Drops



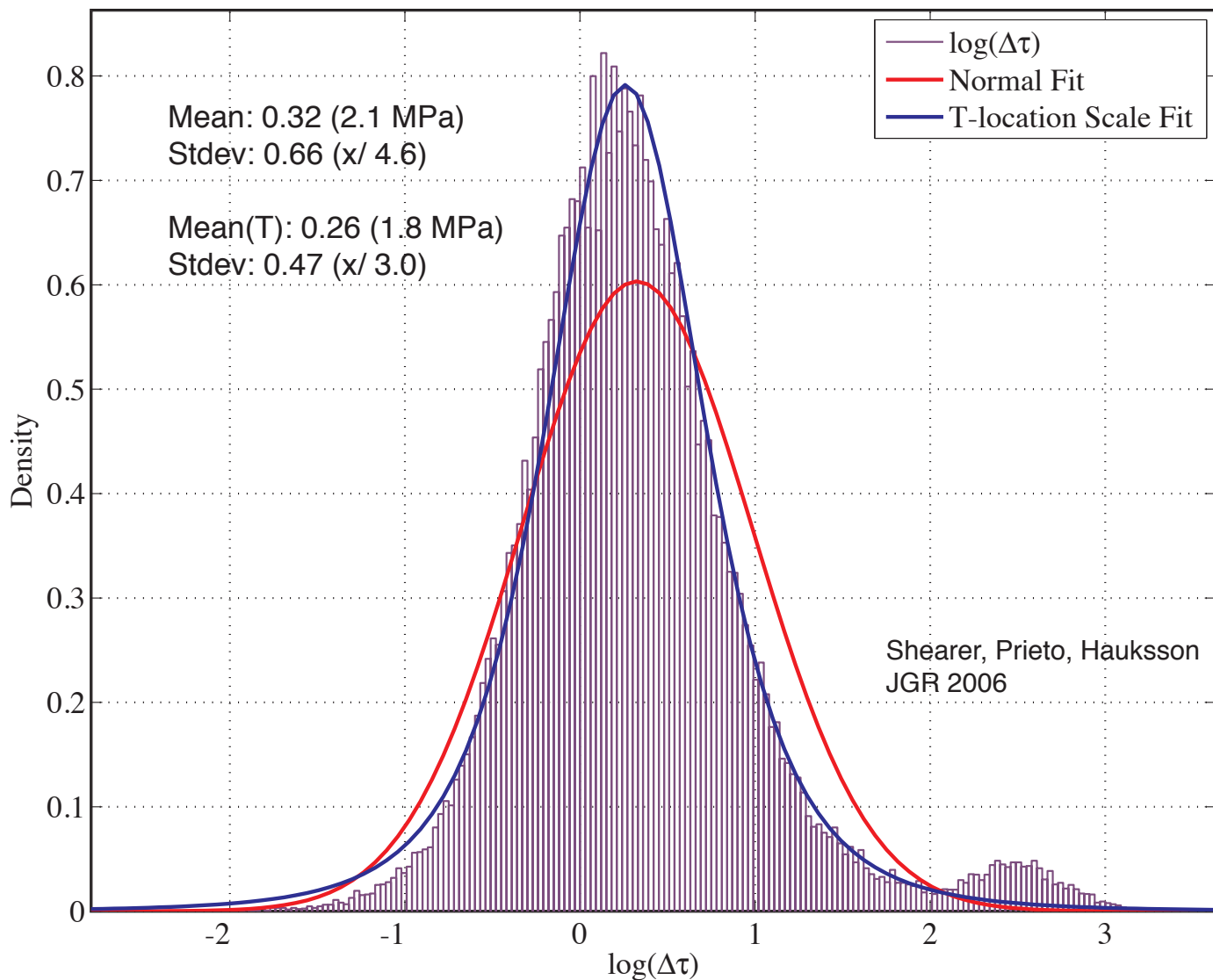


Southern California: M_0 vs f_c



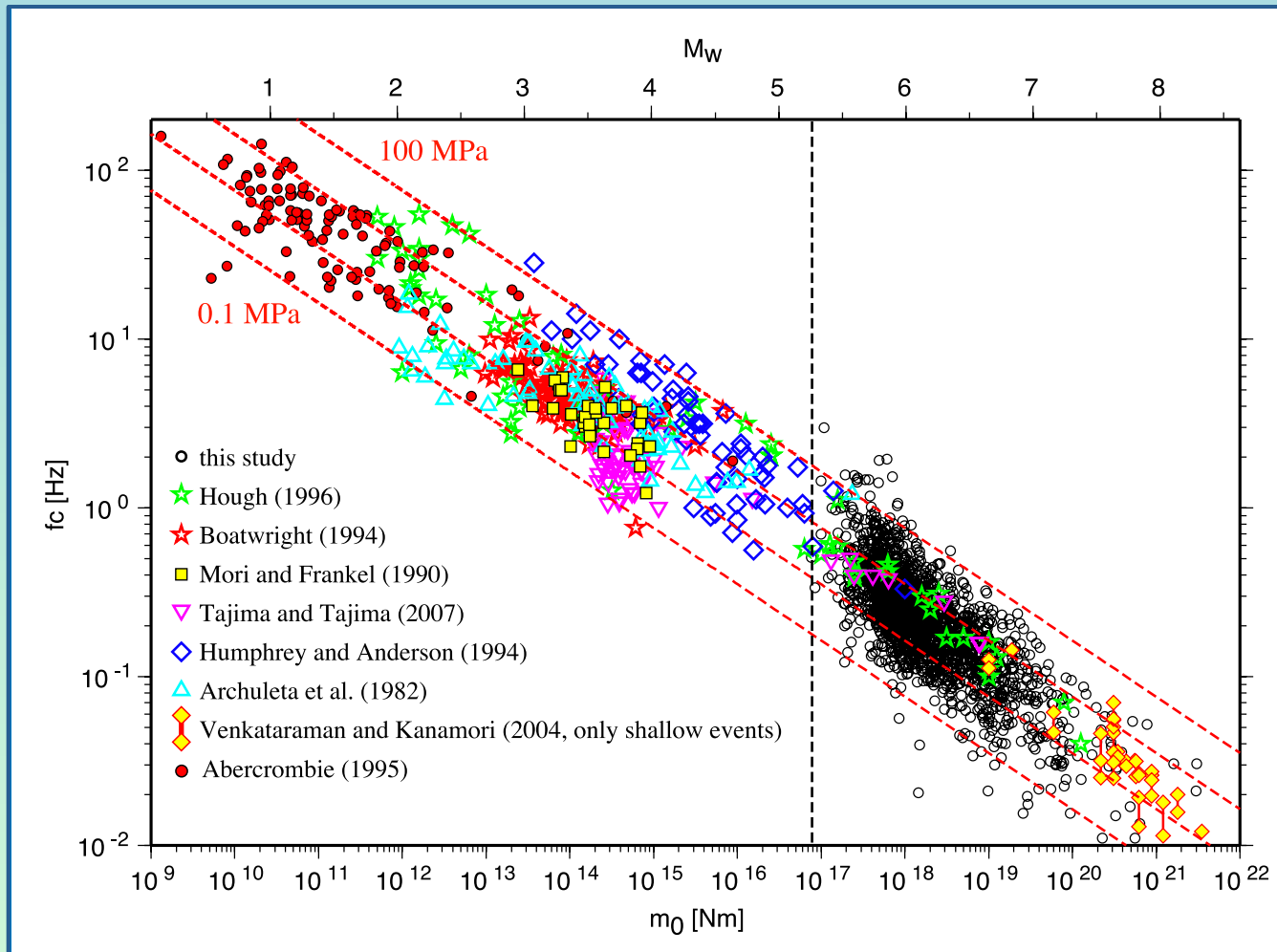


Southern California: $>60,000$ with $M_L = 1.5$ to 3.1



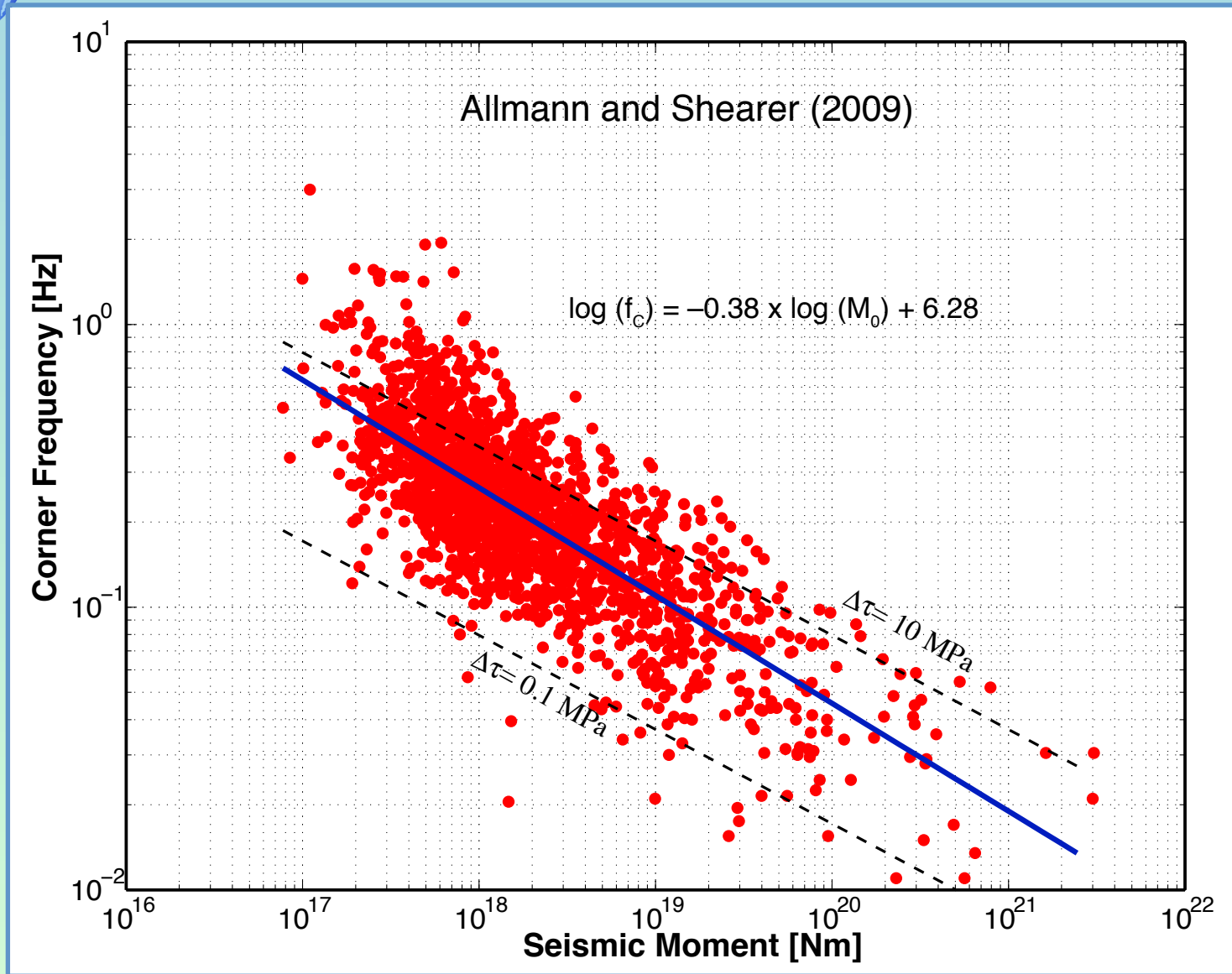


Stress Drop: $10^9 \leq M_0 \leq 10^{22}$ Nm



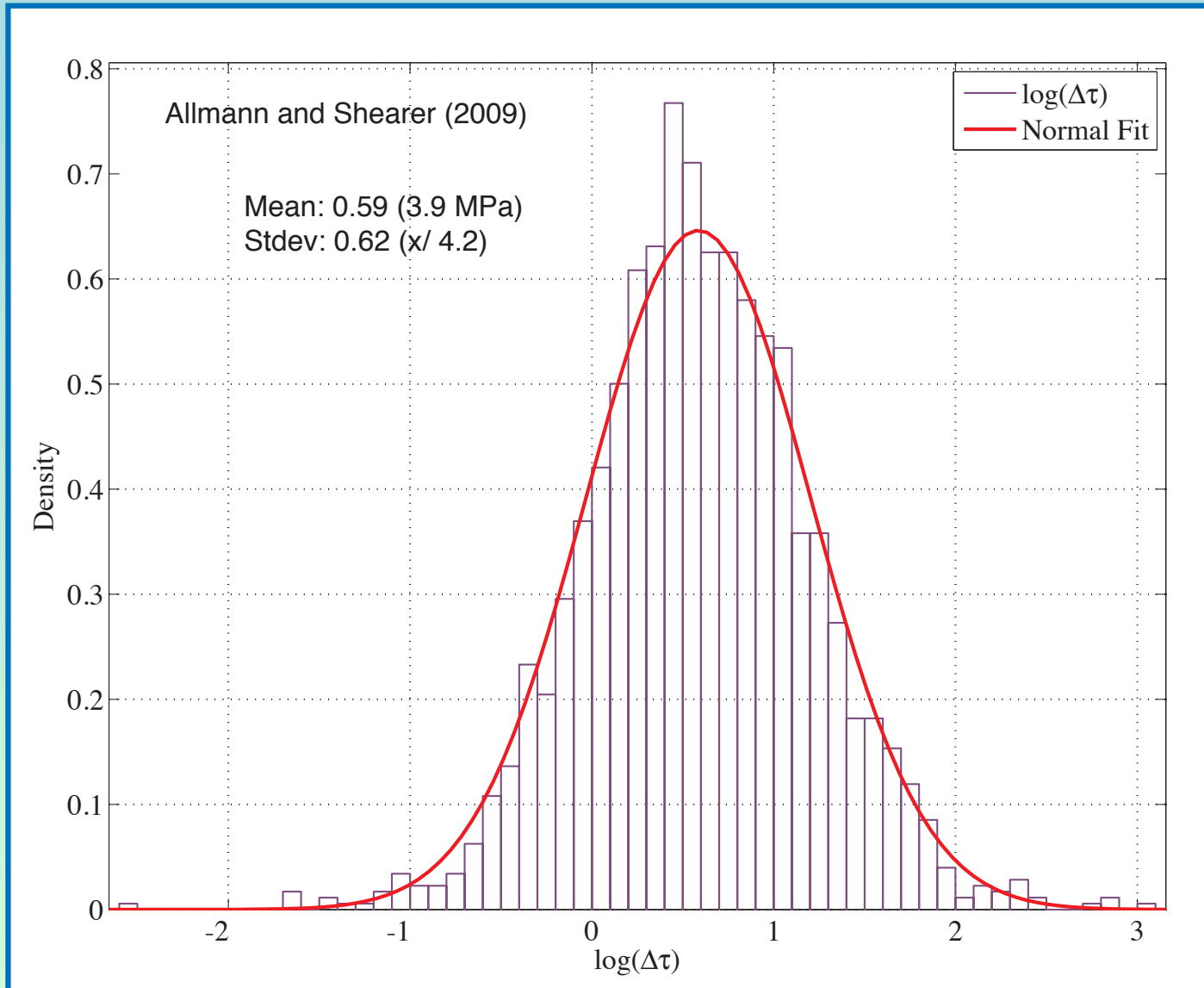


Global Earthquakes: M_0 vs f_c



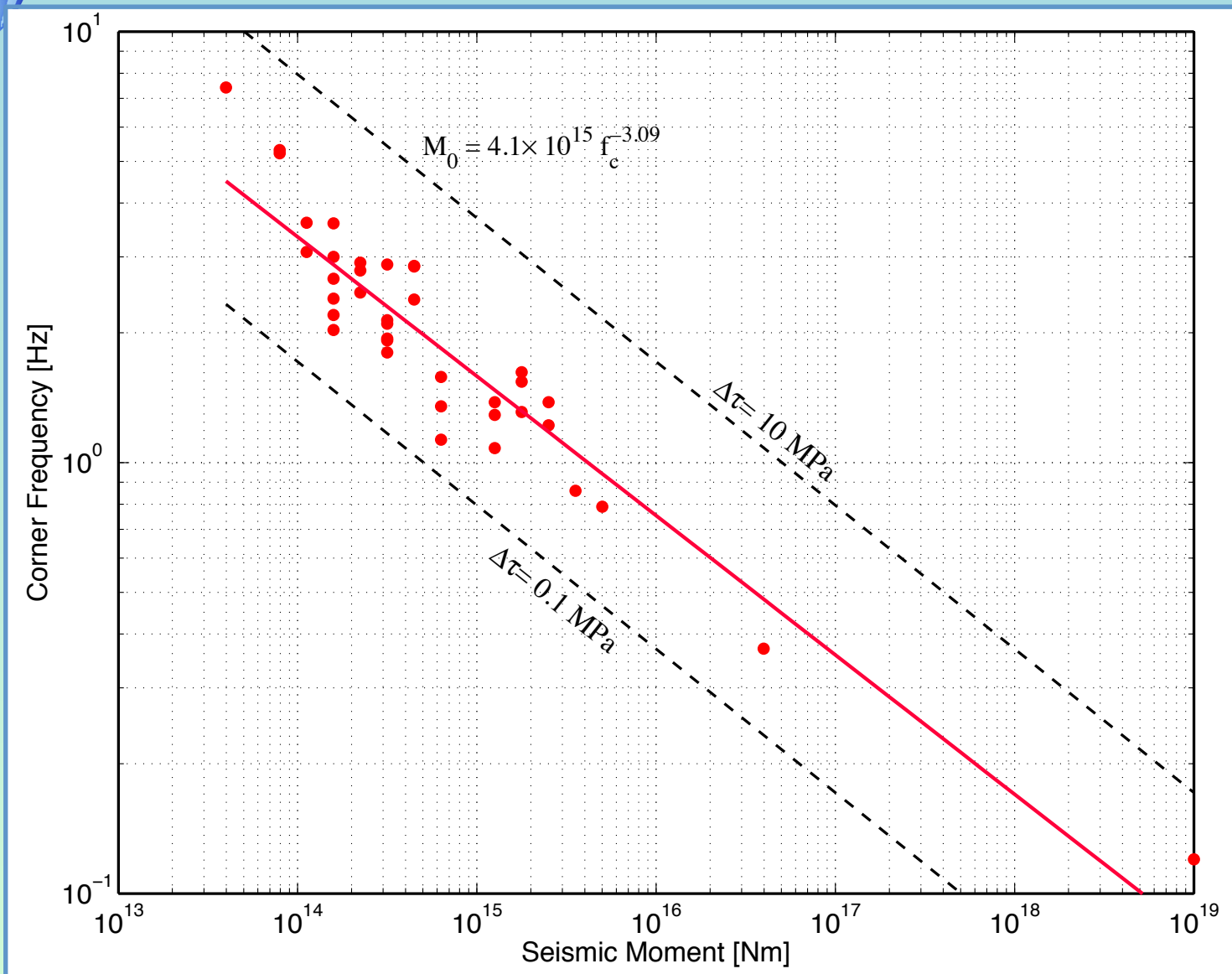


Distribution of Stress Drop



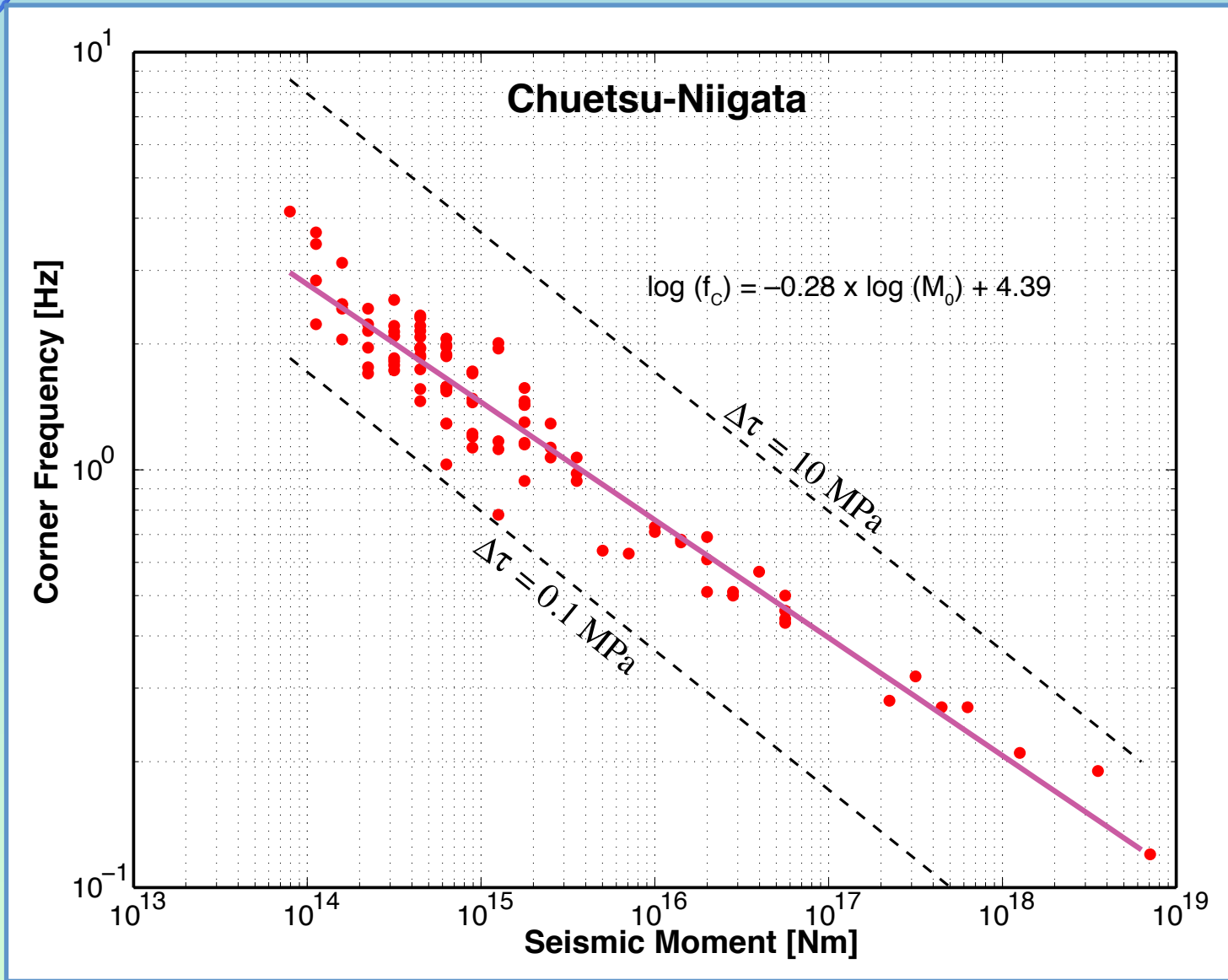


Tottori: M_0 vs f_c



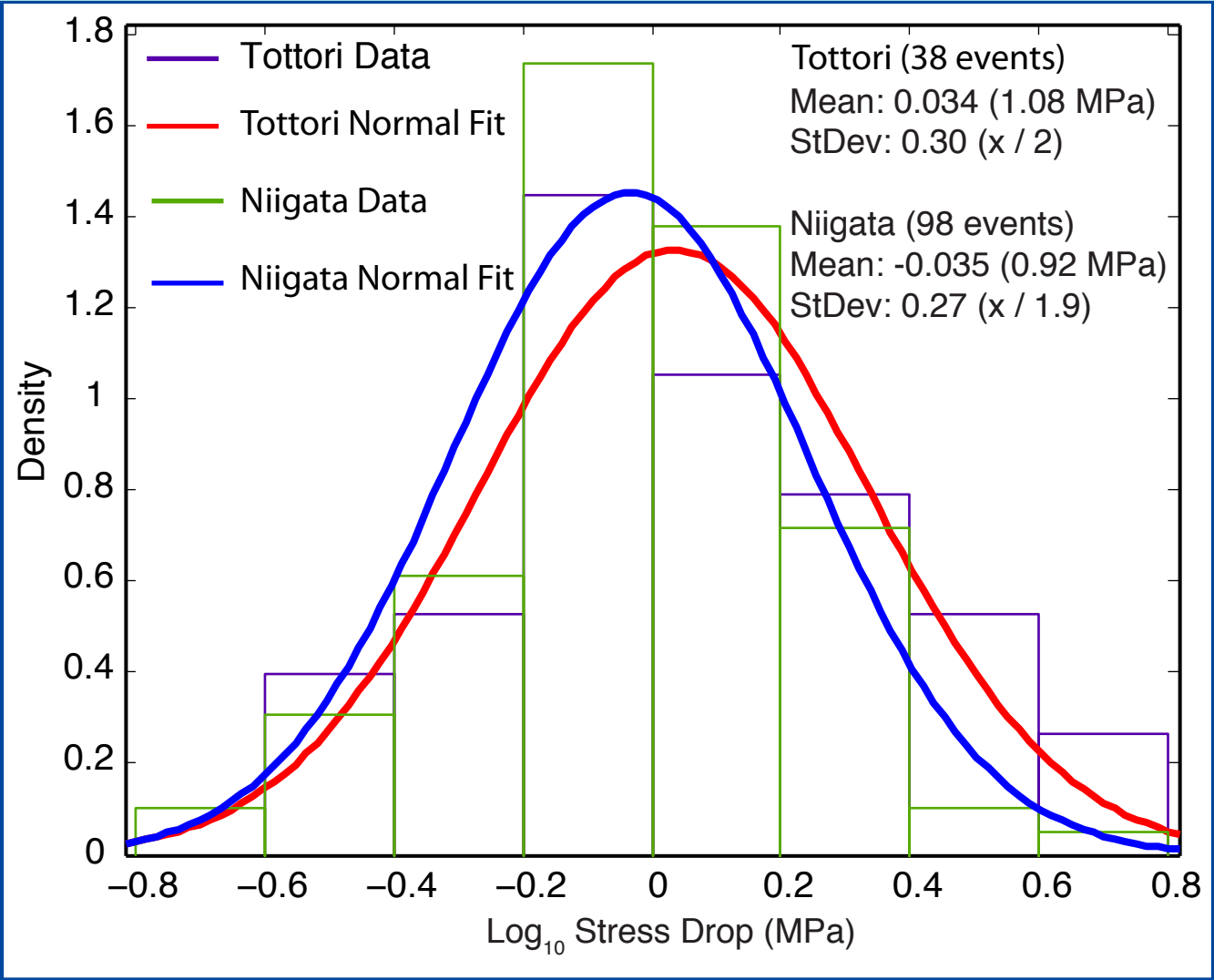


Chuetsu-Niigata: M_0 vs f_c





Normal Distribution: Chuetsu-Niigata and Tottori





Stress Drop and Variability from Spectral Studies (M_0, f_c)

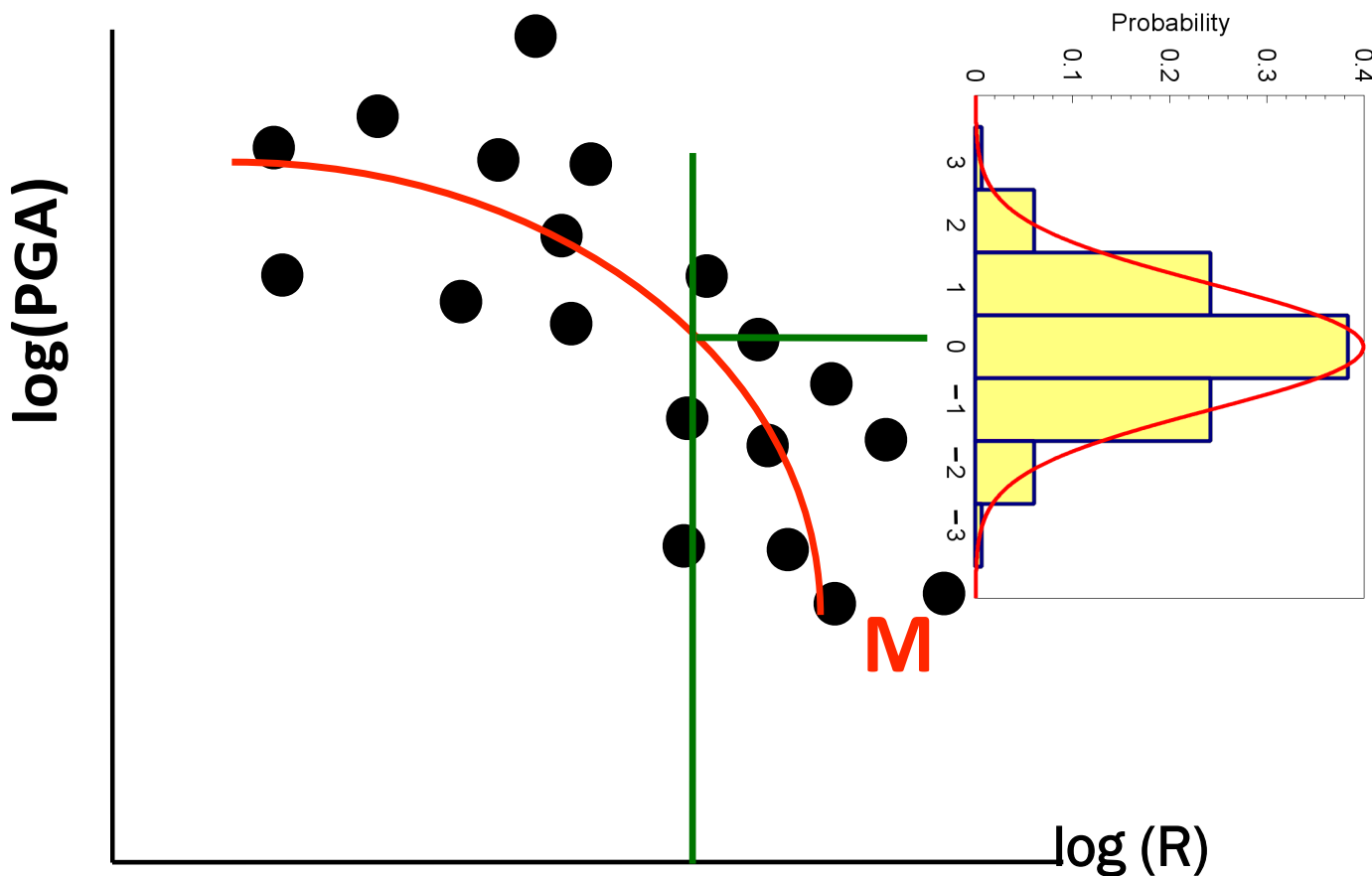
Source study	Region	Mean Brune stress-drop (MPa)	Stress-drop variability (Natural log)	No. earthquakes
Allmann and Shearer, 2009	Interplate $5.5 \leq M_W \leq 8$	0.84*	1.67	799
Allmann and Shearer, 2009	Intraplate $5.5 \leq M_W \leq 8$	1.50*	1.46	61
Oth et al, 2010	Japan (crustal) $2.7 \leq M_{JMA} \leq 8$	1.1	1.38	1951
Rietbrock et al., 2012	UK	1.8	1.38	273
Edwards and Fah, 2012	Switzerland (foreland)	0.2	1.83	161
Edwards and Fah, 2012	Switzerland (alpine)	0.12	1.43	351
Shearer et al., 2006	Southern California $1.6 \leq M_L \leq 3.1$	0.52*	1.52	64800
Margaris and Hatzidimitriou, 2002	Greece $5.2 \leq M_W \leq 6.9$	6.3	0.57	18
Johnston et al., 1994	Intraplate	10	0.7	?

*Published results are divided by 3.95 to take into account the difference between a Madariaga (1976) corner frequency/source radius compared to that of Brune (1970,1971) and the difference in shear wave velocity.



Variability in GMPE's

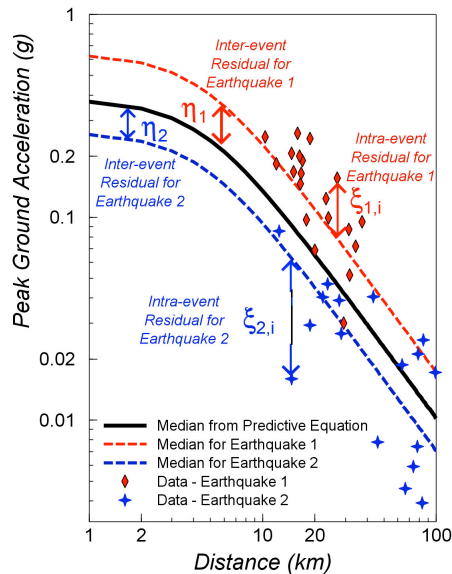
The logarithmic residuals are generally found to conform to a normal distribution with mean 0 and standard deviation σ_T





Variability in GMPE's

Method 2 : analyze the observed ground-motion variability



$$\sigma_T^2 = \sqrt{\sigma_b^2 + \sigma_w^2}$$

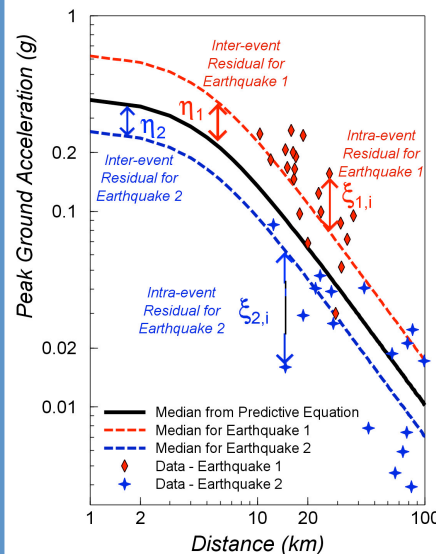
σ_T is the total variability

σ_b is the between-event (earthquake-to-earthquake) variability

σ_w is the within-event (record-to-record) variability

Strasser et al. (2009)

Method 2 : analyze the observed ground-motion variability



The between-event (earthquake-to-earthquake) variability (σ_b) is «on the first order» controlled by the stress-drop variability ($\sigma_{\ln(\Delta T)}$)

Strasser et al. (2009)



Inferred Stress Drop Variability from Recent GMPE's

GMPE	Database	Observed Between Event Variability (Natural log)	Inferred Stress Drop Variability (Natural log)
Rodriguez-Marek et al., 2011	Japan	0.49	0.59
Abrahamson and Silva, 2008 (M=5)	NGA	0.42	0.50
Abrahamson and Silva, 2008 (M=6)	NGA	0.36	0.43
Abrahamson and Silva, 2008 (M=7)	NGA	0.35	0.42
Akkar and Bommer, 2010	Europe	0.23	0.28
Boore and Atkinson, 2008	NGA	0.26	0.31
Campbell and Bozorgnia, 2008	NGA	0.22	0.26
Chiou and Youngs, 2008 (M=5)	NGA	0.34	0.41
Chiou and Youngs, 2008 (M=6)	NGA	0.30	0.36
Chiou and Youngs, 2008 (M=7)	NGA	0.26	0.31
Zhao et al., 2006	Japan	0.40	0.48



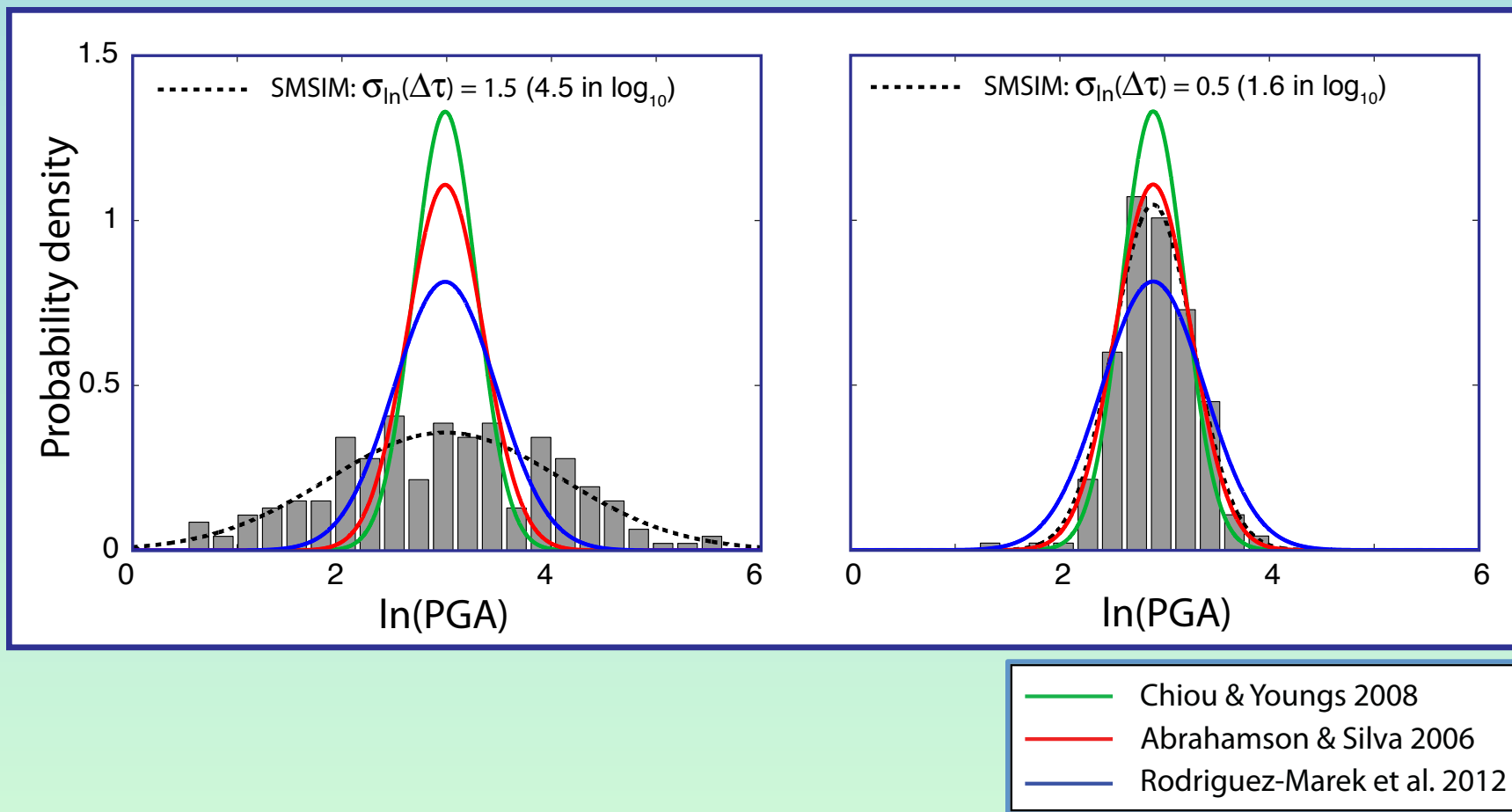
Comparing Variability from Source Studies and Inferred from GMPE's

Generally a factor ~3-4

Source Studies Stress Drop Variability (Log10)		GMPE Inferred Stress Drop Variability (Log 10)
3.85	No one-to-one comparison	1.36
3.36		1.15
3.18		0.99
3.18		0.97
4.21		0.64
3.29		0.71
3.50		0.60
1.31		0.94
1.61		0.83
		0.71
		1.11



Sigma: Its Effect on Ground Motion





Error in Corner Frequency Drives Variability in Stress Drop

$$\Delta\tau = 7 M_0 / 16 r^3$$

$$\Delta\tau = (7/16) M_0 f_C^3 / (k V_s)^3$$

$$\log \Delta\tau = \log \left[7/16 (k V_s)^3 \right] + \log M_0 + 3 \log f_C$$

$$\zeta = \log \Delta\tau$$

$$\sigma_\zeta^2 = \sigma_\chi^2 + 9\sigma_\lambda^2$$

$$\sigma_{\log(\Delta\tau)}^2 = \sigma_{M_0}^2 + 9\sigma_{f_C}^2$$

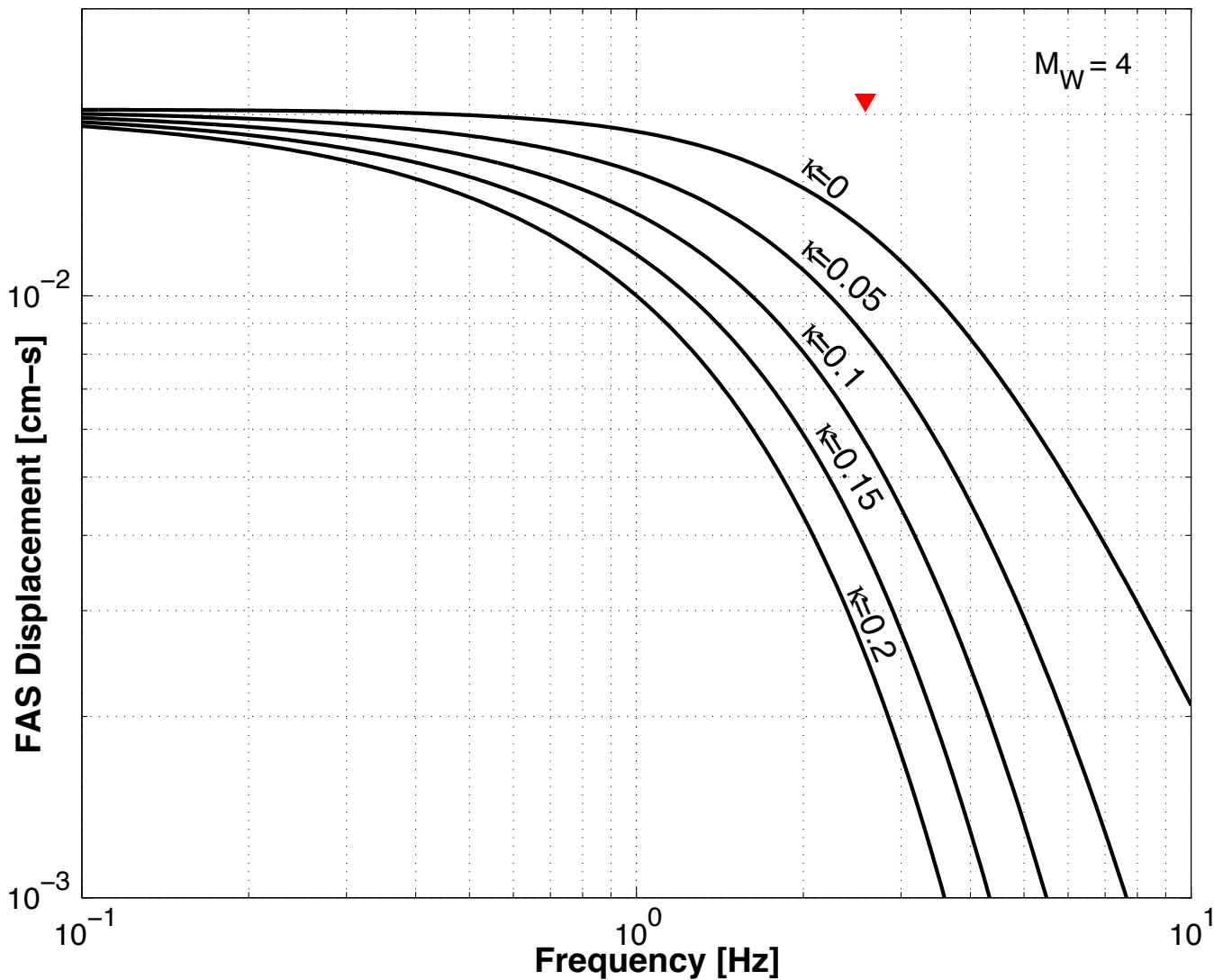
$$\sigma_\zeta^2 = (0.3)_\chi^2 + 9(0.3)_\lambda^2$$

$$\sigma_\zeta^2 = 0.09 + 0.81$$

$$\sigma_\zeta = \sigma_{\log \Delta\tau} = 0.95$$

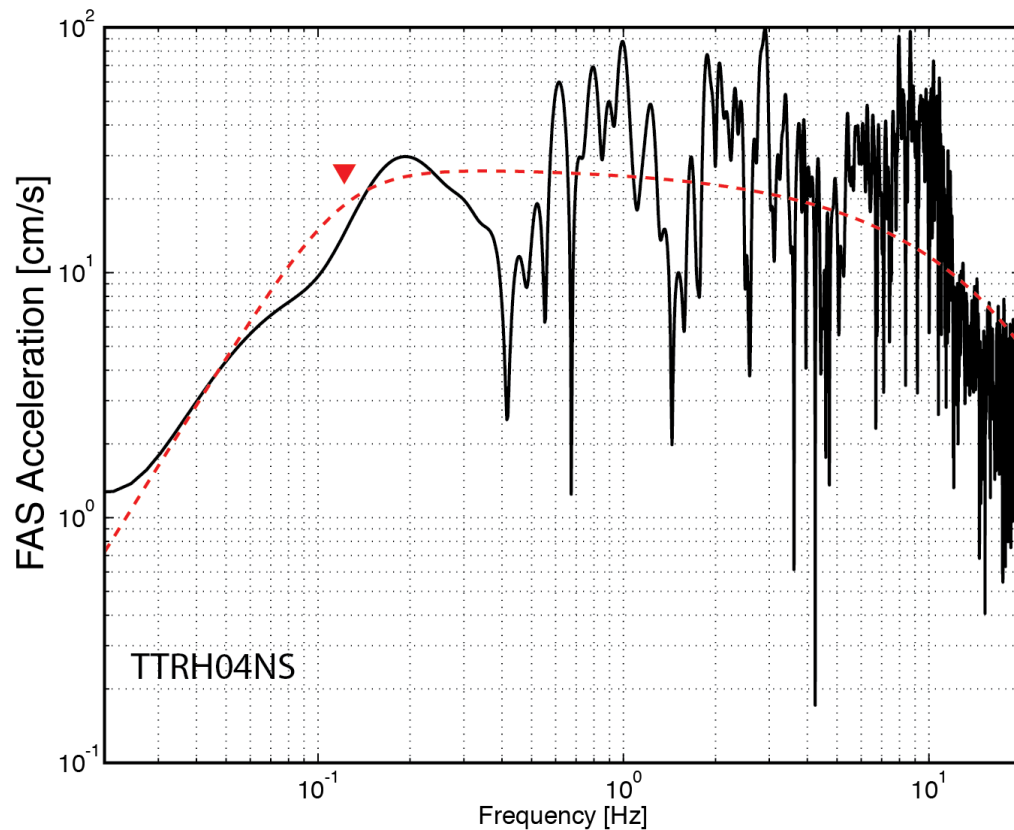


Effect of Attenuation





Stress Drop Based on Root-Mean-Square Acceleration



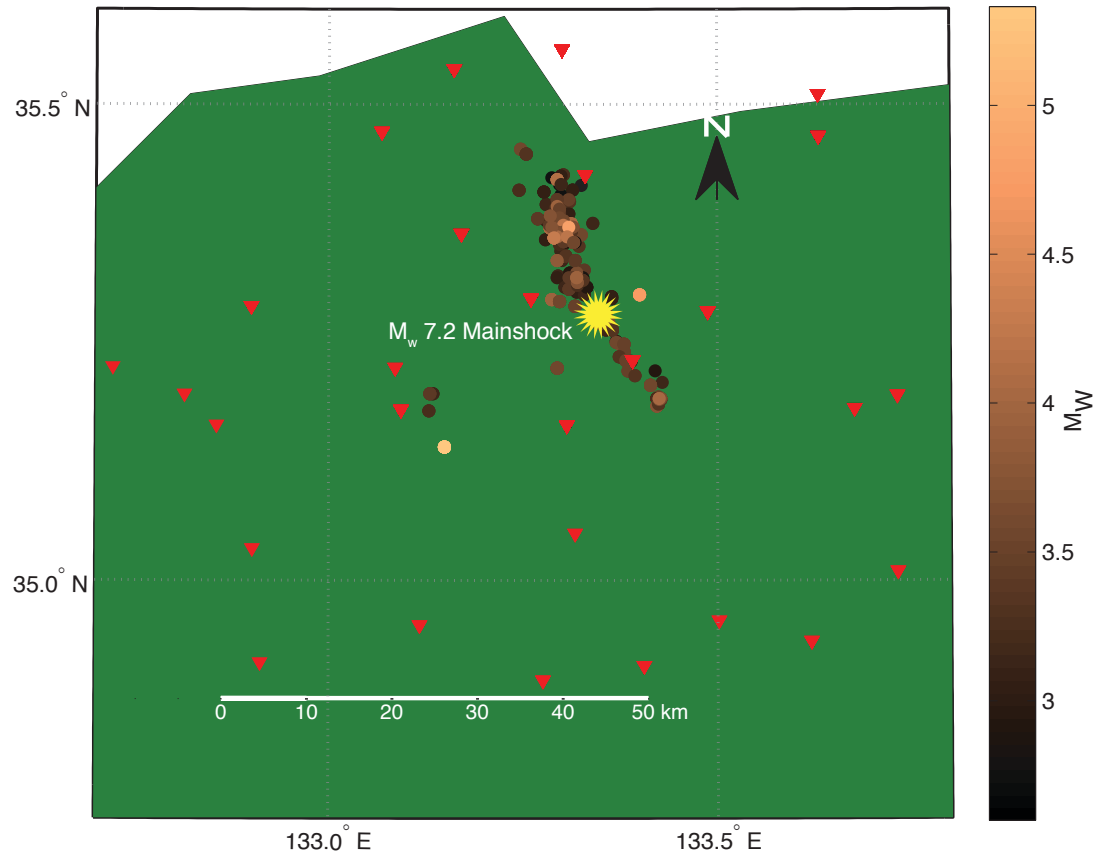
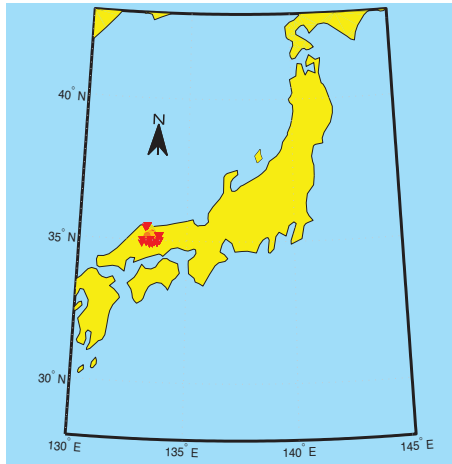
$$a_{rms} = \frac{(2\pi)^2 \Delta\tau}{106\rho R} \sqrt{\frac{f_{\max}}{f_C}}$$

$$f_{\max} = QV_S / \pi R$$

$$\Delta\tau = \frac{a_{rms} 106\rho R}{(2\pi)^2} \sqrt{\frac{f_C}{f_{\max}}}$$

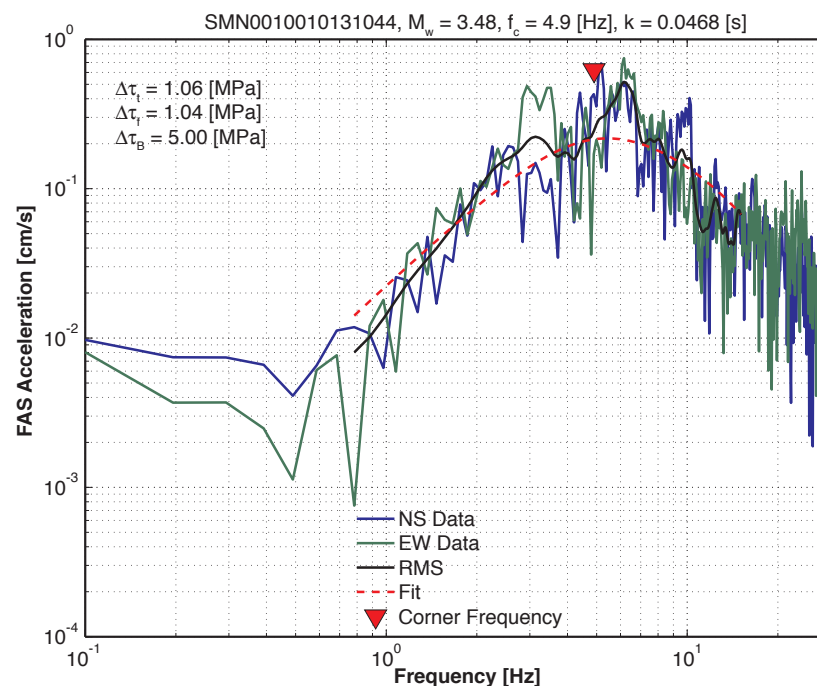
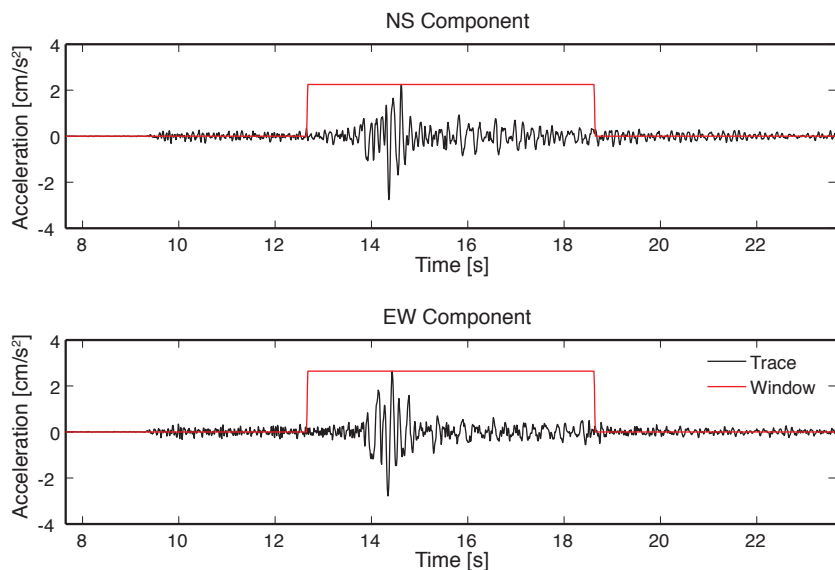


Map of Tottori Earthquake



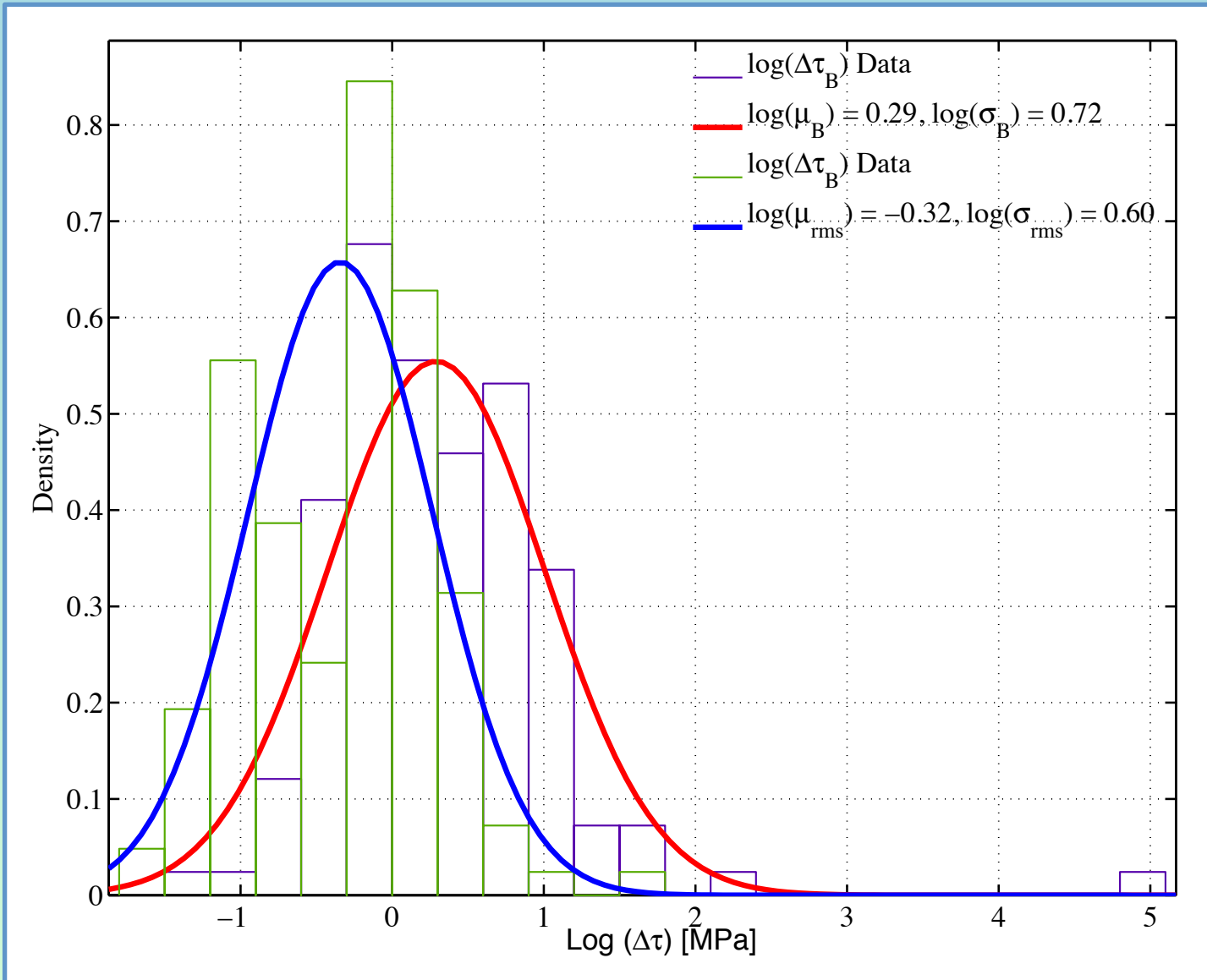


Root-Mean-Square Acceleration





Tottori: Stress Drop Distribution





Summary

- The real variability in stress drop is less than that found using the standard Brune analysis of the seismic spectrum, i.e., corner frequency and spectral level at “0” frequency.
- Variability of the stress drop is real. There is a regional dependence of the mean and could be in the variability.
- In theory, using root-mean-square acceleration should provide a more reliable estimate of the variability in stress drop.
- Attenuation (path and site) plays a significant role in both the standard Brune analysis as well as analysis of the root-mean-square spectrum.

The End





Variability of Stress Drop Derived from Variability of GMPE

$$PGA = a_{rms} \sqrt{2 \ln(2 f_{\max} T_D)} = a_{rms} \sqrt{2 \ln\left(\frac{2 f_{\max}}{f_C}\right)}$$

$$T_D = 1 / f_C$$

$$PGA = \frac{(2\pi)^2 \Delta\tau}{106 \rho R} \sqrt{\frac{f_{\max}}{f_C}} \sqrt{2 \ln\left(\frac{2 f_{\max}}{f_C}\right)}$$

$$\Delta\tau = (7/16) M_0 f_C^3 / (k V_s)^3$$

shows

$$\sqrt{1/f_C} \propto 1/\Delta\tau^{1/6}$$

Thus

$$PGA \propto \Delta\tau^{5/6}$$

$$\sigma_{\Delta\tau} = (6/5) \sigma_{PGA}$$