

EAN**P**LATE**O**BSERVING**S**YSTEN





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Multi-hazard and multi-risk assessment for geohazards

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#### **■ F F F A Forward Probabilistic Framework (PTRA)**



Behrens, J., Løvholt, F., Jalayer, F., Lorito, S., Salgado-Gálvez, M.A., Sørensen, M., Abadie, S., Aguirre-Ayerbe, I., Aniel-Quiroga, I., Babeyko, A. and Baiguera, M., 2021. Probabilistic tsunami hazard and risk analysis: A review of research gaps. *Frontiers in Earth Science*, *9*, p.628772.





#### The definition of the fragility

In the context of risk assessment at at regional level, the fragility curve is defined as the probability of exceeding a specific damage level as a function of the intensity measure.

$$P(D > D_i | IM = im)$$



# There are some implicit assumptions in the definition of fragility

It is meaningful for a **single system**. It is assumed that with each new event of interest, the system will be "renewed" back to its intact state  $(D_0)$ .

#### Why Class Fragility?

Short of detailed buildingto-building level information, class fragilities are useful for loss analysis at the regional (portfolio) level.

#### The concept of fragility curve for a class

The fragility curve for a class can be derived by assuming that the portfolio of buildings in a class is replaced by an "average" representative building. The dispersion in the class fragility curve, in theory, should consider the:

(1) Variability in the "events" (e.g., tsunamis, earthquakes) given the intensity measure;

(2) The building-to-building variability within the class;

#### H R Class Fragility Analysis using Small-sample MC Simulations

EF)

Ε



Simulations are used to estimate the fragility parameters and not the of extremes, therefore, even a small-sample (in the order of 50-100) Monte Carlo Simulation could work.

#### Across EPOS TCS's: Analytical Class Fragility Assessment



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Tsunami TCS Tools

**BED** Tools

#### **EF**) **EFH EKample: Archetype Building**

**Storey Height:** Ground floor = 2.9 m Upper floor = 2.65 m

#### Taxonomy: CR\_LFINF-CDL-0\_H2

Building type selected based on the exposure model of Catania, Italy. Designed by the **simulated design** package:

- Geometry
- Details of reinforcement
- $\circ$  One-way slab
- High construction quality
- Concrete strength  $f_{ck} = 14$  MPa
- Steel yield strength  $f_{syk} = 400 \text{ MPa}$





	Classification	Threshold
DS0	Slight	$\theta_{\rm DS0} = 0.75 \theta_{\rm y}$
DS1	Moderate	$\theta_{\rm DS1} = 0.5\theta_{\rm y} + 0.33\theta_{\rm c}$
DS2	Extensive	$\theta_{\rm DS2} = 0.25\theta_{\rm y} + 0.67\theta_{\rm c}$
DS3	Complete	$\theta_{\rm DS4} = \theta_{\rm c}$

 $\theta_{\rm y}$  = yield rotation  $\theta_{\rm c}$  = rotation at 20% strength drop

Crowley, H., Dabbeek, J., Despotaki, V., Rodrigues, D., Martins, L., Silva, V., Romão, X., Pereira, N., Weatherill, G. and Danciu, L., 2021. European seismic risk model (ESRM20). *EFEHR Technical Report*, *2*.

<sup>±</sup>UC

EFEH R



A total of 92 scenarios were generated by INGV, 60 out of which were used for this fragility analysis.





Gibbons, S.J., Lorito, S., Macías, J., Løvholt, F., Selva, J., Volpe, M., Sánchez-Linares, C., Babeyko, A., Brizuela, B., Cirella, A. and Castro, M.J., 2020. Probabilistic tsunami hazard analysis: high performance computing for massive scale inundation simulations. *Frontiers in Earth Science*, *8*, p.591549.







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#### **Tsunami Loading**

3D nonlinear model built in **OpenSees Sumami loads include:** • **Hydrostatic** load: F = pgbh;• **Hydrodynamic** load:  $F = \frac{1}{2}pcdb(hu^2);$ • Time-history analysis based on the 60 • Time-history analysis based on the 60 • Bi-directional taumani wave • Infilis assumed to break when the flow depth reach their mid-height

### 3D nonlinear model built in *OpenSees* Tsunami loads include:

- **Hydrostatic** load:  $F = \rho g b h$ ;
- Hydrodynamic load:  $F = \frac{1}{2}\rho C_{d}b(hu^{2});$
- Time-history analysis based on the 60 tsunami scenarios (transient solver)
- Bi-directional tsunami wave
- Infills assumed to break when the flow depth reach their mid-height





#### Tsunami Fragility: Flow Depth Modified Cloud Analysis (MCA)



Jalayer, F., Ebrahimian, H., Miano, A., Manfredi, G. and Sezen, H., 2017. Analytical fragility assessment using unscaled ground motion records. *Earthquake Engineering & Structural Dynamics*, *46*(15), pp.2639-2663.

## **■** F) E H R Tsunami Fragility: Momentum Flux







Comparisons with Japan 2storey RC building:

- Damage scales are Ο different
- The analytical curve has Ο no building-to-building variability

Flow depth (m)

4

2

0

Geo

()

Source: European Tsunami Risk Service

 $DS_4$ 

DS<sub>1</sub> Emp

DS<sub>2</sub> Emp

DS<sub>3</sub> Emp

 $DS_{4}$  Emp

6

8

https://github.com/eurotsunamirisk/etris\_data\_and\_data\_products/blob/main/etris\_data\_products/bl cts/Fragility Curves/Japan%202011%20RC%2C%202%20storey M1.csv

#### Some take home points

A simulation-based procedure for class fragility assessment.

The models can be sophisticated since small-sample MC simulation is used.

Challenges related to harmony of definitions (taxonomy, damage scale, design, modelling.

Access to ground motion recordings and tsunami inundation simulations.

Importance of detailed exposure models to model building-to-building variability.

Challenges in geolocalising the building classes on the map for simulation purpose (not always available).