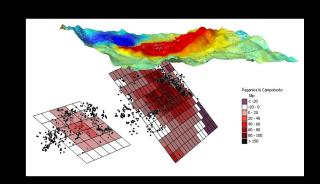
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# Stress drop variability and dynamic fault weakening for extended earthquake sources

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#### **Key Talking Points**

- Reconciling seismological measurements, geological observations and the key findings of laboratory experiments
- 2 Model dependence. Estimated parameters are model dependent and they do not allow us to distinguish the processes controlling dynamic fault weakening
- 3 Scale dependence: implications for selfsimilarity

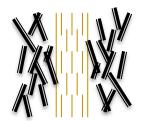
## Focus: Fault Zone Physical Processes during Seismic Slips

- How does *shear stress* ( $\tau$ ) vary with *slip* ( $\delta$ ) during earthquakes?
  - (Focus is on *large* slip, *e.g.*,  $\delta > 0.1$  m, well beyond slips of order 0.01 mm to 0.5 mm at which events are thought to *nucleate*)
- What physical mechanism of weakening during slip?
  - (Argued here: Different physical mechanisms can control dynamic weakening each of which has its own spatial and temporal length scales)
- What fracture energy (G) is implied by the  $\tau vs. \delta$  relation?
  - (Important because *seismological fracture energy* is different from fracture energy *in fracture mechanics*)

### (1) Lessons from geological observation



- Fault zone structure is complex:
  - volumetric versus surface processes



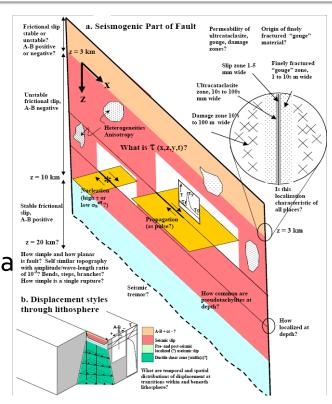
- Complex damage zones: energy loss outside the slip zone.  $G' = W_b = W_{on} + W_{off}$   $V_{peak} \le V_{limit}$ 
  - Impact on <u>fracture energy</u> and <u>peak slip velocity</u>.
- Structure of the fault core
  - impact on hydraulic and thermal properties
- Principal slipping zones (strain localization)
  - have a finite, although small, thickness
  - and are geometrically complex.

#### (1) Lessons from seismology

- Seismological investigations rely on a phenomenological description of source parameters
- We measure global source parameters
  - $M_o$ ,  $E_R$ ,  $\sigma_a$ ,  $D_{av}^{100\%}$ , Fault Area: A=L•W,  $M_L$
- We measure macroscopic parameters (on a virtual mathematical plane of zero thickness)
  - $\Delta \sigma_s(\xi)$ ,  $\Delta \sigma_d(\xi)$ ,  $\Delta \tau_b(\xi) = \tau_y(\xi) \tau_o(\xi)$ ,  $V_r(\xi)$ ,
  - $D_{tot}(\xi)$ ,  $D_{mean}^{\neq \%}$ ,  $D_{max}$ ,  $V_{peak}(\xi)$



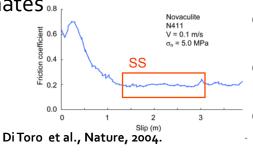
Breakdown Work W<sub>b</sub> or seismological fracture energy G'

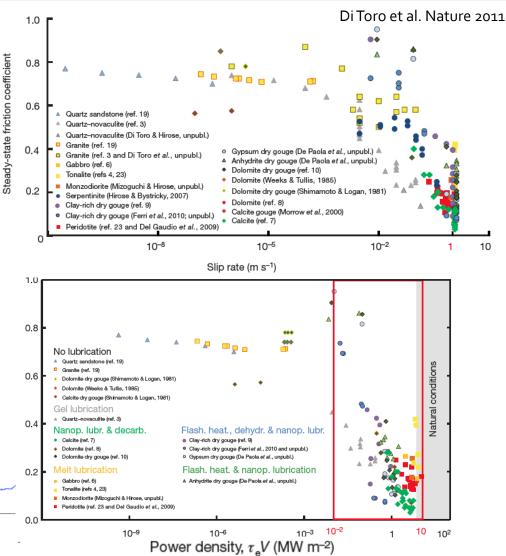


from Dahelm Workshop report (2005)

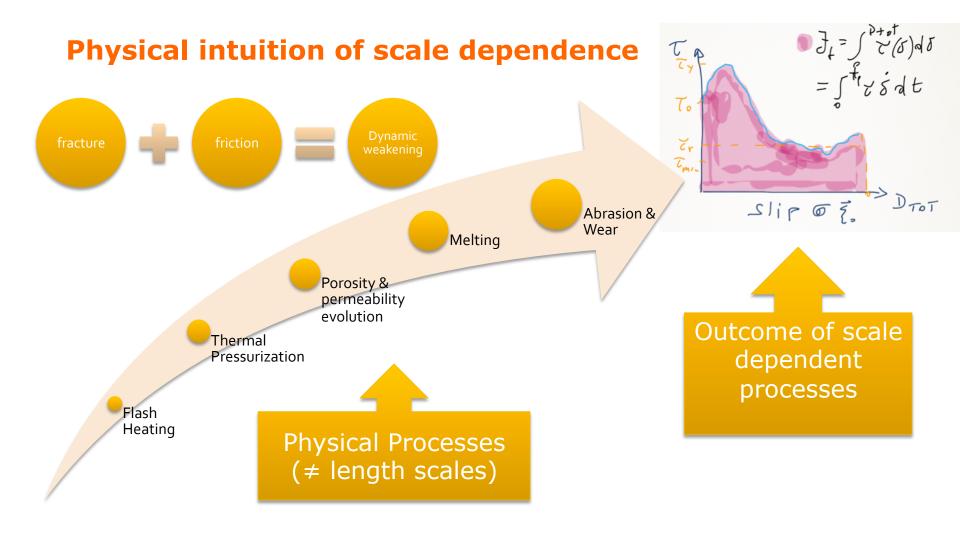
#### (1) Lessons from Lab experiments

- Lab experiments show dynamic fault weakening
- Efforts are still needed to bridge the gap between natural and experimental faults
- HVFE have the advantage of:
  - produce similar experimental and natural fault products
  - generate similar mechanical work estimates...



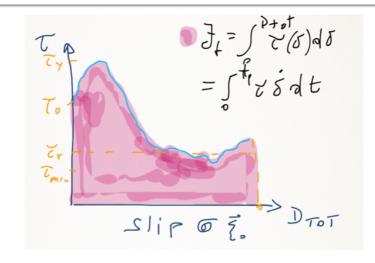


#### **Dynamic Fault Weakening**

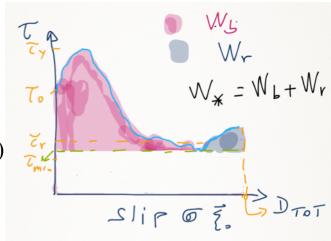


#### The Macroscopic Frictional Work

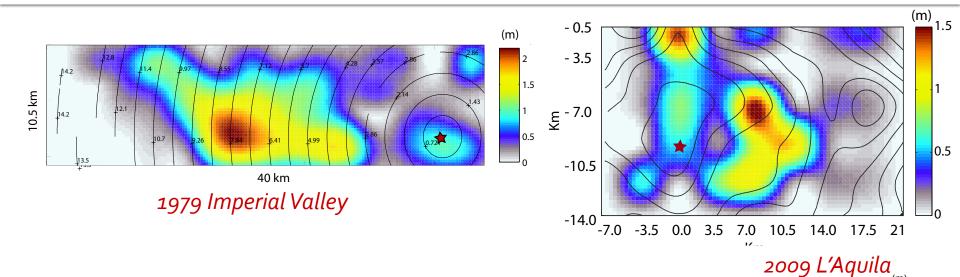
We have defined the macroscopic frictional work as the irreversible part of mechanical work, which is the work that does not go into elastic strain energy and kinetic energy, and it is partitioned into surface energy and heat (here for heat we mean all the distinct dissipative mechanisms such as high frequency stress waves, plastic deformation on- and off-fault)



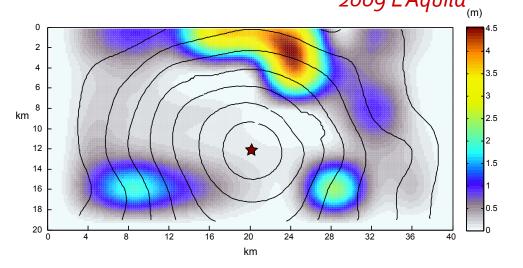
Work Rate 
$$\tau_i \Delta \dot{u}_i = \sum_{l} + \Delta q$$
 Frictional Work 
$$\Im(\vec{\xi}) = \int_0^{t_m} \tau_i \Delta \dot{u}_i dt = \int_o^{D_t} \tau_i d(\Delta u_i)$$
 Total Frictional Work 
$$\Delta E_{\Sigma} = \iint_{\Sigma} dS \int_0^{t_m} \tau_i \Delta \dot{u}_i dt = \iint_{\Sigma} dS \int_o^{D_t} \tau_i d(\Delta u_i)$$
 Breakdown Work 
$$W_b = \int_0^{T_b} (\vec{\tau}(t) - \vec{\tau}_{\min}) \cdot \dot{\delta}(t) dt$$



### Kinematic rupture models imaged from geophysical data inversions



Rupture histories are used to constrain the traction evolution and to infer dynamic rupture parameters as well as seismological fracture energy.



2000 Western Tottori

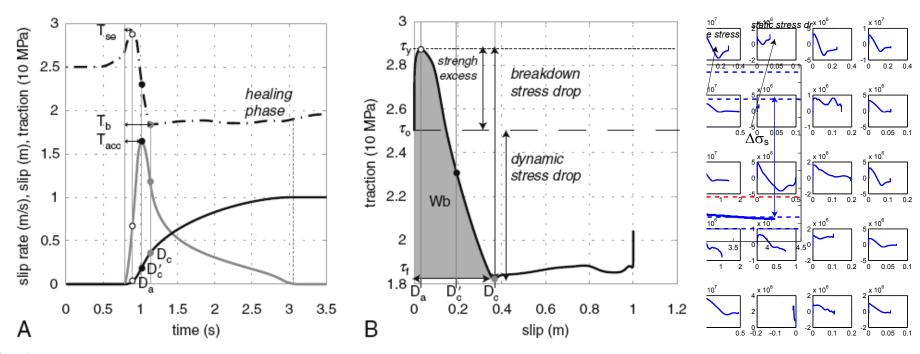
### Estimates of dynamic parameters for real earthquakes

We infer the traction change evolution on the fault plane by using the rupture history

We solve the Elastodynamic equation using the slip velocity history as a boundary condition on the fault

$$\sigma(x,t) = -\frac{\beta}{2\mu}\Delta \dot{u}(x,t) + \iiint \Delta \dot{u}(\xi,\tau) K(x-\xi,t-\tau) d\xi d\tau$$
 Fukuyama & Madariaga (1998) 
$$\Delta \dot{u}(\xi,t) = \dot{f}(t-t_r(\xi)) \cdot d(\xi)$$
 Slip Velocity time history on the fault 
$$\underbrace{\xi}_{\text{Tinti}} = \underbrace{\xi}_{\text{Tinti}} =$$

#### Reconstructing stress evolution

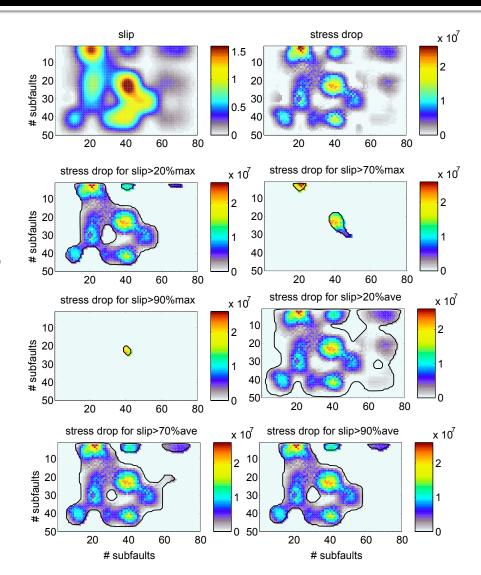


**FIGURE 1** (a) Comparison of slip velocity, slip, and traction time histories at a target point on a fault plane using a smoothed Yoffe function as a source time function. Black solid circles indicate the time of peak slip velocity ( $T_{\rm acc}$ ) and the gray solid circles indicate the end of weakening ( $T_b$ ). (b) Corresponding traction versus slip behavior; the same circles of panel a are used to indicate the parameters  $D_a$ ,  $D'_c$ , and  $D_c$ .

Cocco M., E. Tinti, C. Marone & A. Piatanesi (2009),

#### Averaging on the fault plane

- For a scale-independent model we can average local estimates of stress drop on different fault portions
- These different average values yield a variability up to a factor 5 in stress drop
- Including k<sup>-2</sup> heterogeneities and assuming scaleindependence confirms and partially enhance such variability



#### (2) Model Dependence

- Stress drop can be inferred from
  - Seismic moment and source radius
  - Brune stress drop: ground acceleration high frequency plateau
  - Rupture history through quasi-dynamic models
- > Stress drop estimates are strongly model dependent

$$r = C \frac{\beta}{f_c}$$
  $\Delta \sigma = \frac{7}{16} \frac{M_0}{r^3}$   $M_0 f_c^3 \approx const \propto \Delta \sigma$ 

(Equations derived assuming circular source with constant rupture velocity)

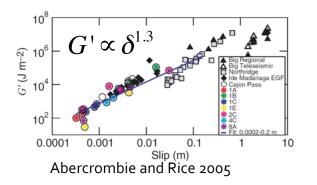
Stress drop from quasi-dynamic models varies on the fault plane and averaging is allowed only for scaleindependent models

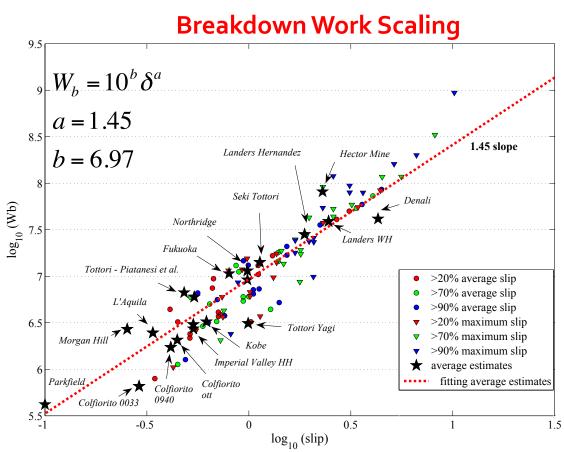
#### Scaling of breakdown work with slip

$$\tau(\delta) = \tau_* + C\delta^n$$

$$W_b = G' = \frac{\partial \tau}{\partial \delta} = Cn\delta^{n-1}$$

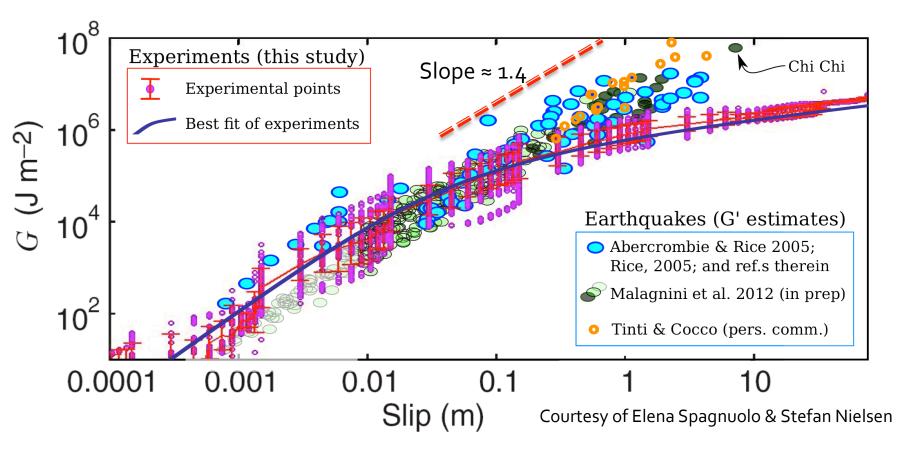
 $\tau A(\delta)$  we  $\tau_{p}$  and  $\tau_{b} \exp(-\alpha \delta / \delta_{1})$  Good for scale-dependence?  $G' = \Delta \tau_{b} \delta_{1}$ 





Regression computed using average values

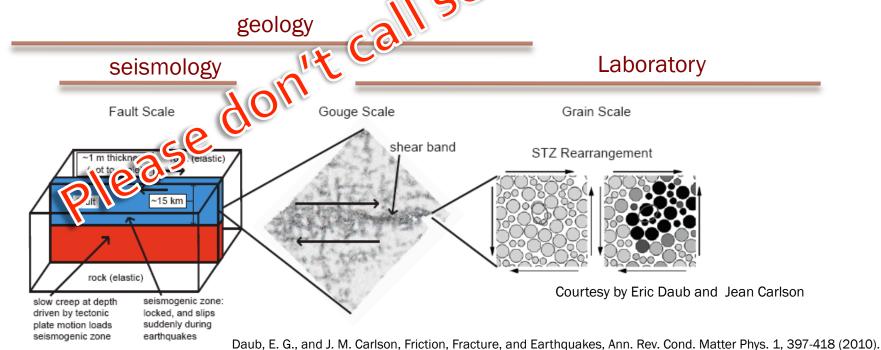
#### Comparison with lab estimates



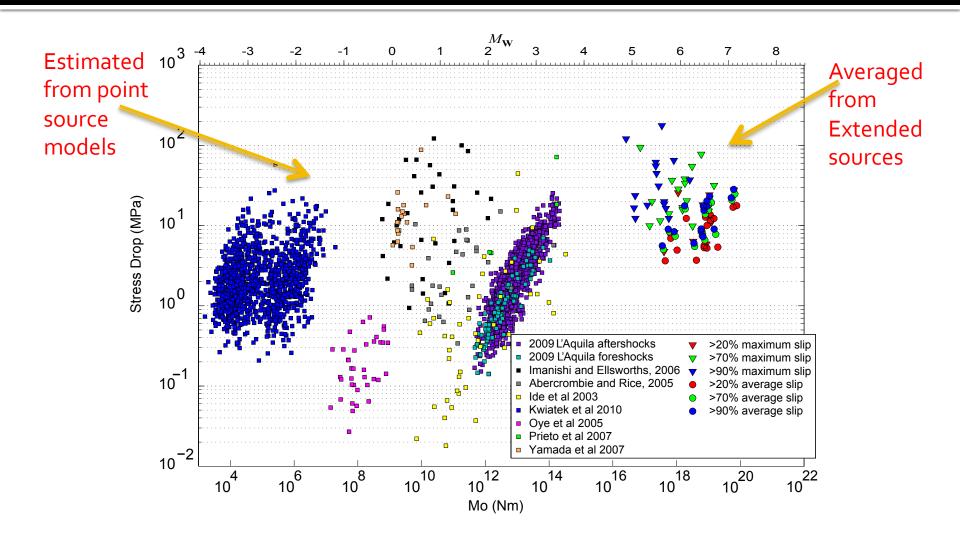
Nielsen et al. 2012. See Friday morning talk.

#### (3) Scale dependence

- In a scale-dependent model, averaging is not allowed and we should apply physically coherent approach to deal with different lengths-scales.
- Asserting self-similarity of earthquake ruptures implies that will be established a hierarchy among length-scale parameters characterizing (2): process and that a single length-scale dominates the others.
- Such a demonstration has never been achiecally far!



### Stress drop scaling with seismic moment



#### Conclusions

- We need a next generation of laboratory derived constitutive laws, which will allow us to study individual physical processes and understanding scale dependence
- Our estimates of source parameters have a large variability and are strongly model dependent
- Paradoxes might be created by ill-posed physical questions
- Are we sure that self-similarity in earthquakes is formulated in a physically coherent way?
   Earthquake size is not a constitutive length scale parameter!

#### **Dynamic Fault Weakening**

Physical intuition of scale dependence

#### Which length-scale dominates for corroborating self-similarity?

 $\tau = g_1(\delta, \delta, \vartheta, p, T, \omega, \kappa, \psi_i, L_1)$ 

